

Synthesis of a Novel Fuel Additive Solketal Levulinate by using MOF ZIF-8 and SSA Loaded PVA Functional Catalytic Membrane

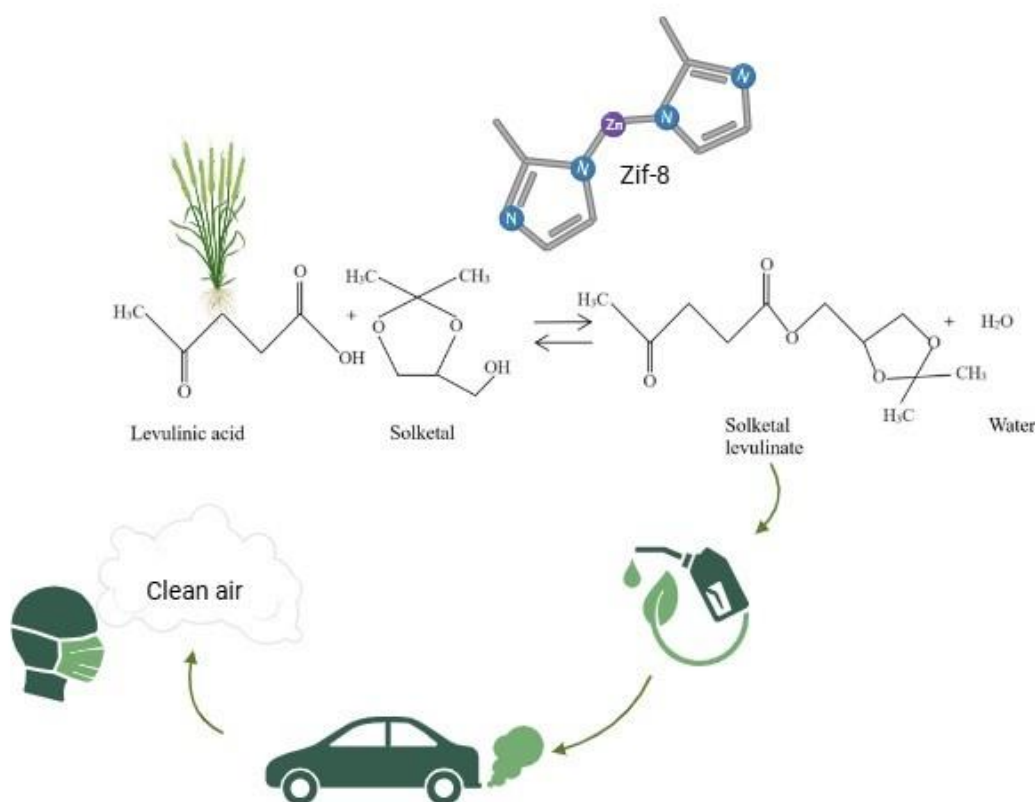
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Graphical abstract



Abstract

Solketal levulinate (SoLE), a potential fuel additive that can improve the physicochemical properties of the fuel, was produced by the developed catalytic membrane from solketal and levulinic acid. The catalytic membrane was prepared in film form as a metal-organic framework of ZIF-8 supported on a sulfosuccinic acid-loaded hydrophilic polyvinyl alcohol polymer. Removing by-product water from the reaction medium with the sorption of the highly hydrophilic membrane contributed to the

conversion. PVA/SSA and PVA/SSA/ZIF-8 membranes were analyzed by FTIR and TGA. ZIF-8 was photographed and analyzed by SEM and XRD, respectively. Higher water affinity of the functional catalytic membranes was calculated by swelling degree and interaction parameter calculations. SoLE synthesis was conducted in the batch reactor under mild conditions. The parameters such as catalyst amount, temperature, solketal/levulinic acid initial molar ratio (M), and reaction time, were investigated. The PVA/SSA catalytic membrane showed a maximum reaction conversion of 97.65% with 105°C, 9 mmol SSA, and an M:6/1 ratio for 6 h. For the PVA/SSA/ZIF-8 catalytic membrane, maximum reaction conversion of 96.81% was obtained at 105°C, with an M:6/1 ratio and 9 mmol SSA for 4 hours. ZIF-8 reduced the reaction time and contributed to the system in terms of efficient energy use.

Keywords: Esterification, levulinic acid, heterogeneous catalyst, Bio-additive

1. Introduction

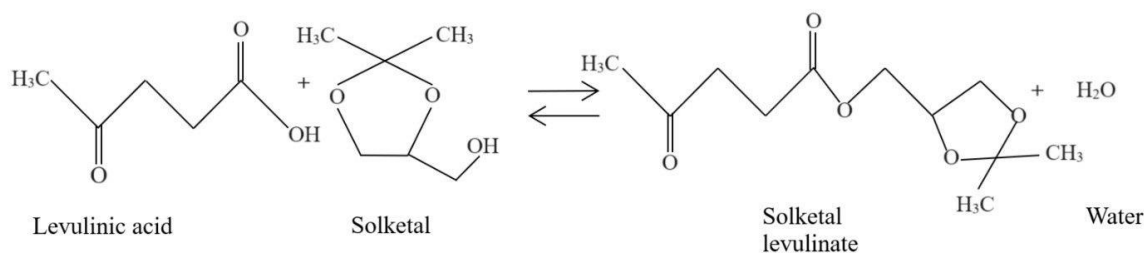
The need for energy reserves in the world is rapidly increasing in direct proportion to the growing human population. Fossil fuel reserves are in danger of exhaustion, which has increased the search for alternative fuels to satisfy energy needs. Interest in the development of green(clean)-content fuels has increased at the outset of a wide range of studies in this direction, as they are both environmentally friendly and renewable resources (Singh et al., 2023). The major problem related to combustion events of bio-based and green-content fuels, which are frequently investigated in the literature, is a key focus of research. Whether the fuels/fuels additive are fossil or green and sustainable fuels, the production of new generation fuel additives to improve the combustion properties of these fuels is an important step towards solving this problem. Toxic emissions from the combustion of fuels are reduced by optimizing engines and equipment, using catalytic converters, NO_x reducers, and particulate filters for engine-based uses, as well as modifications to the chemical composition of the fuels (Çakmak and Özcan, 2018). In addition to conventional methods (isomerization, catalytic cracking, reforming-dehydrocyclization), oxygen-rich fuel additives and oxygenates can be added to improve the octane number of gasoline and the cetane number of diesel. However, traditional methods

43 are costly and difficult. The octane number of gasoline or the cetane number of diesel are improved
44 by adding oxygenates such as oxygenated alcohols and ethers after the refining of crude oil (Demirbas
45 et al., 2015). Bio-ethanol, which is the leading bio-based fuel additive, can be obtained chemically or
46 through fermentation. However, in both situations, long-term production processes cause both carbon
47 emissions and system costs to increase. This makes the production process less environmentally
48 friendly (Mussatto et al., 2010). Commonly encountered levulinate-based oxygenates in the literature
49 include ethyl levulinate, methyl levulinate, and SoLE. However, these levulinate-based fuel additives
50 are mainly produced by the reaction of alcohols or ketals with oxo-carboxylic acid anions (methyl
51 levulinate, ethyl levulinate, etc.) (Jia et al., 2020). In such reactions, alcohols are used as reactants or
52 as by-products, and these alcohols (except ethanol) are highly toxic and ecologically hazardous (Xu
53 et al., 2020). Solketal levulinate (SoLE) is a potential levulinate-based fuel additive that improves the
54 cold flow properties of the fuel (Mariam et al., 2024; Mariam et al., 2021). As shown in Fig. 1, SoLE
55 can be synthesized from solketal and levulinic acid (Sutinno, 2016). This reaction, levulinic acid
56 esterification, is a very environmentally friendly reaction in terms of both reactants and products. In
57 addition, it produces no harmful waste. There are very few studies in the literature on the synthesis
58 of SoLE from solketal and levulinate esters. In this study, SoLE was synthesized from solketal and
59 levulinic acid for the first time. Levulinic acid (LA), a 5-carbon ketoacid, is one of the twelve platform
60 chemicals defined by the US Department of Energy that can be produced from biomass; an
61 environmentally friendly alternative to petroleum-based chemical production (Jeanmard et al., 2025).
62 There are numerous commercial chemicals produced from LA, such as aminolevulinic acid (DALA),
63 diphenolic acid (DPA), methyl tetrahydrofuran, various esters, and resins. Fuel additives can also be
64 synthesized from LA, a highly versatile building block chemical. (Sajid et al., 2021; Ethiraj et al.,
65 2022). Solketal, which is also used as a reactant in its synthesis, is a renewable and green solvent and
66 can be used alone as an environmentally friendly fuel additive (Fernández et al., 2019; Ilgen et al.,
67 2017). Polyvinyl alcohol (PVA) is a highly hydrophilic, biocompatible, environmentally friendly,
68 functional synthetic polymer that can form good films. Due to its high hydrophilicity in reactions

69 where water is a by-product, PVA can provide sorption support to the reaction to remove the by-
70 product and direct the reaction equilibrium to the product side (Song et al., 2023; Unlu and Hilmioglu,
71 2019). Sulfosuccinic acid (SSA), which can be bio-based and sustainable, is a highly effective catalyst
72 when added to the catalytic membrane, especially in esterification reactions due to its acidic nature
73 (Portillo Perez et al., 2023). Zeolitic imidazolium framework-8 (ZIF-8), used as a support material in
74 the catalytic membrane, is a type of metal-organic framework (MOF). MOFs are porous materials
75 comprised of organic ligands and metal ions. They can be used as catalyst supports with their high
76 specific surface area, microporosity, and finely tunable chemical and physical properties (Doan et al.,
77 2025; Wi'sniewska et al., 2023; Laeim et al., 2025). Catalytic membranes, which are environmentally
78 friendly functional catalysts, often composed of polymeric matrices and catalysts, are bifunctional
79 materials that direct the reaction equilibrium towards product formation by removing the by-product
80 of the reaction through sorption support (Hasirci et al., 2023). Studies on the synthesis of SoLE are
81 very limited in the literature, and the synthesis was carried out by a transesterification reaction using
82 a base catalyst. Mariam et al., 2021 synthesized SoLE from solketal and methyl levulinate as a
83 potential fuel additive for palm biodiesel. They achieved a maximum yield of 74.83% at 140°C and
84 1.5% catalyst loading with Methyl levulinate/Solketal at a molar ratio of 1:4 for 6 hours. Liu et al.,
85 2024, produced methyl levulinate glycerol ketal from methyl levulinate and glycerol. The influence
86 of different parameters on methyl levulinate glycerol ketal yield and glycerol conversion were
87 investigated. The optimum conditions were determined as temperature $T = 140\text{ }^{\circ}\text{C}$, catalyst loading
88 of 0.50 g HZSM-5, and ML/GLY mol ratio of 4:1. Under these conditions, glycerol conversion was
89 97%, and methyl levulinate glycerol ketal yield was 94.7%. SoLE can be manufactured by acid-
90 catalyzed esterification of solketal and levulinic acid (Mariam et al., 2021; Sutinno, 2016).
91 Esterification reactions are processes in which water is produced as a by-product (Moradi et al.,
92 2021). Water removal from the reaction medium shifts the equilibrium towards the products and
93 increases the reaction conversion (Hilmioglu, 2022). For the first time in the literature, SoLE was
94 synthesized from solketal and levulinic acid in a batch reactor using a catalytic membrane. Blending

95 catalysts used in the reaction with suitable polymer solutions to convert them from homogeneous to
96 heterogeneous form is an excellent way to produce catalytic membranes. In this study, ZIF-8, used as
97 a support material with an MOF cage structure was synthesized, functionalized with sulfosuccinic
98 acid (SSA) with high Brönsted acid sites, and blended with PVA polymer to prepare catalytic
99 membranes. In the context of SoLE production, green catalytic membranes have not been used in the
100 literature before. Reactions with catalytic membranes are hybrid systems in which both the reaction
101 with the catalyst and the separation of the desired product or by-product, according to the properties
102 of the membrane material used (hydrophilic or hydrophobic), from the environment can be performed
103 simultaneously in a single unit. For this reason, the contribution of this research article, to the
104 literature, is promising for future studies.

105 This study established an experimental batch reactor system by placing catalytic membrane pieces
106 inside. Ease of operation and re-use of the catalyst is enabled by the batch reactor, in which the
107 reaction and sorption of the by-product occur simultaneously. This shifts the reaction balance towards
108 the product and increases conversion without using extra reactants. The reaction was shown in Fig. 1



109
110 **Fig. 1** Solketal levulinate synthesis from Levulinic acid and Solketal (Sutinno, 2016)
111

112 2. Materials and Methods

113 2.1. Materials

114 PVA in solid form (MW~125,000), SA (70% in water), and 2-methylimidazole were obtained from
115 Sigma-Aldrich; zinc nitrate hexahydrate ($\text{Zn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$) was obtained from Acros Organics, while
116 LA (for synthesis) was obtained from Merck Chemicals. Solketal was purchased from BLD Farm.

117 2.2. ZIF-8 synthesis

118 ZIF-8 was synthesized by the rapid addition of an aqueous solution of $\text{Zn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ to an aqueous
119 solution of 2-methylimidazole. Firstly, 1.17 g of zinc nitrate was dissolved in 8 g of distilled water.
120 Then, 22.70 g of 2-methylimidazole was dissolved separately in 80 g of distilled water. These two
121 solutions were combined and stirred at room temperature until a turbid solution was formed. It was
122 then centrifuged, and the ZIF-8 precipitate obtained was dried at 80 °C overnight (Pan et al., 2011).

123 2.3. Preparation of PVA/SSA and PVA/SSA/ZIF-8 Functional Catalytic Membranes

124 3, 6, and 9 mmol of SSA were added respectively to 6% PVA solutions, each prepared in certain
125 predetermined amounts. The PVA-catalyst mixture was stirred for 1 hour and then poured onto Teflon
126 plates and was left to dry. The dried membranes were then heat treated at 120 °C for 1 hour for
127 crosslinking. For the preparation of ZIF-8 doped PVA/SSA membranes, 0.1 g ZIF-8 was added to
128 PVA solutions. After stirring the PVA-ZIF-8 mixture for 1 hour, either 3, 6, or 9 mmol of SSA were
129 added, and the mixture was further stirred. In the last step, PVA/ZIF-8/SSA mixtures were poured
130 onto Teflon plates and left to dry at room temperature. As before, dried membranes were heat-treated
131 at 120 °C for 1 h for crosslinking.

132 2.4. Batch Reactions

133 Solketal levulinate reaction was carried out with PVA/SSA and PVA/SSA/ZIF-8 functional catalytic
134 membranes at 105 °C. The loading of SSA acid catalyst in the catalytic membranes used in the
135 reaction was 3, 6, 9 mmol and the initial molar ratios for Solketal/Levulinic Acid were chosen as 4/1,
136 5/1, 6/1. The batch reactor is shown in Figure 2.

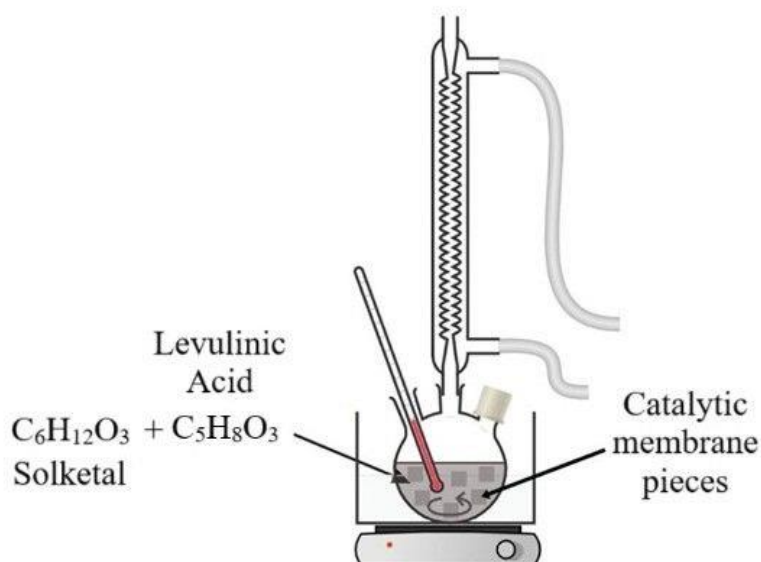


Fig. 2 Batch Reactor system

2.5. Analysis of Reaction Products

The catalytic performance of PVA/SSA and PVA/SSA/ZIF-8 functional catalytic membranes was analyzed by the titration method, with LA conversion calculated by Equation 1 (Unlu and Hilmioglu, 2016)

$$X = \frac{N_{A0} - N_A}{N_{A0}} \quad (1)$$

N_{A0} is the number of moles of levulinic acid in solution at the beginning, and N_A is the number of moles of levulinic acid at any given time.

3. Results and Discussions

3.1. Fourier-transform infrared spectroscopy (FTIR) characterization of PVA/SSA and PVA/SSA/ZIF-8 catalytic Membranes

Fig. 3 shows the FTIR spectra of pure PVA, PVA/SSA, and PVA/SSA/ZIF-8 functional catalytic membranes. The characteristic peak observed at 3260 cm^{-1} wavenumber in pure PVA belongs to the O-H stretching band, while the characteristic absorbance peak at 1096 cm^{-1} is due to the C-O

153 stretching (Khatuua et al., 2015; Norouzi et al., 2021). When PVA/SSA functional catalytic
 154 membranes were examined, the O-H stretching band observed at 3260 cm^{-1} shifted to 3365 cm^{-1} upon
 155 addition of SSA to the structure. (Rynkowska et al., 2019). The peak observed at a wavelength of
 156 1035 cm^{-1} is associated with the stretching vibration of the S-O bond, indicating the presence of SSA.
 157 1725 cm^{-1} represents the C=O bond of SSA (Ngo et al., 2022). For PVA/SSA/ZIF-8, when ZIF-8 was
 158 added to the polymer matrix, it was observed that the peak intensity of the hydroxyl groups in the
 159 structure decreased. This can be explained by the high hydrophobicity of ZIF-8 (Yang et al., 2021).

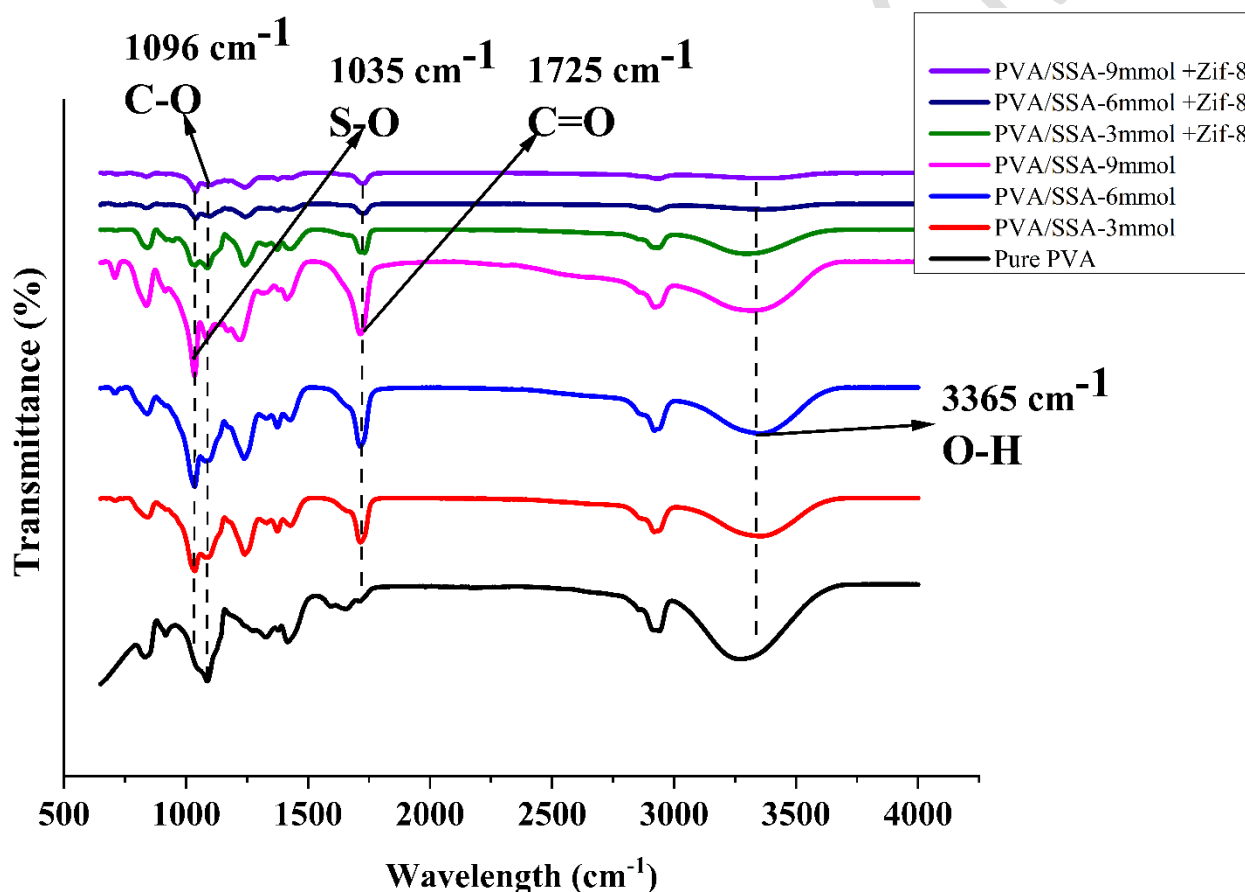


Fig. 3 FT-IR of PVA/SSA and PVA/SSA/ZIF-8 catalytic membranes

3.2. Thermogravimetric analysis (TGA) of PVA/SSA and PVA/SSA/ZIF-8 catalytic membranes

Three degradation regions were observed in the TGA curves of PVA/SSA and PVA/SSA/ZIF-8 catalytic membranes, shown in Fig. 4. While the first degradation in the 100°C - 210°C temperature

range is due to the elimination of water in the structure, the degradation in the second region from 210°C to 300°C is related to the detachment of sulfonic groups from the ester bonds between SSA and PVA. The polymer chain decomposed in the last region (between 420 °C and 500 °C) (Gomaa et al., 2017; Maarouf et al., 2020). According to the TGA curves for PVA/SSA catalytic membranes, SSA added to PVA increased the thermal stability compared to pure PVA. In addition, the amount of residue at the end of the analysis increased directly with the amount of SSA (Rynkowska et al., 2019). No significant effect of ZIF-8 on thermal stability was observed.

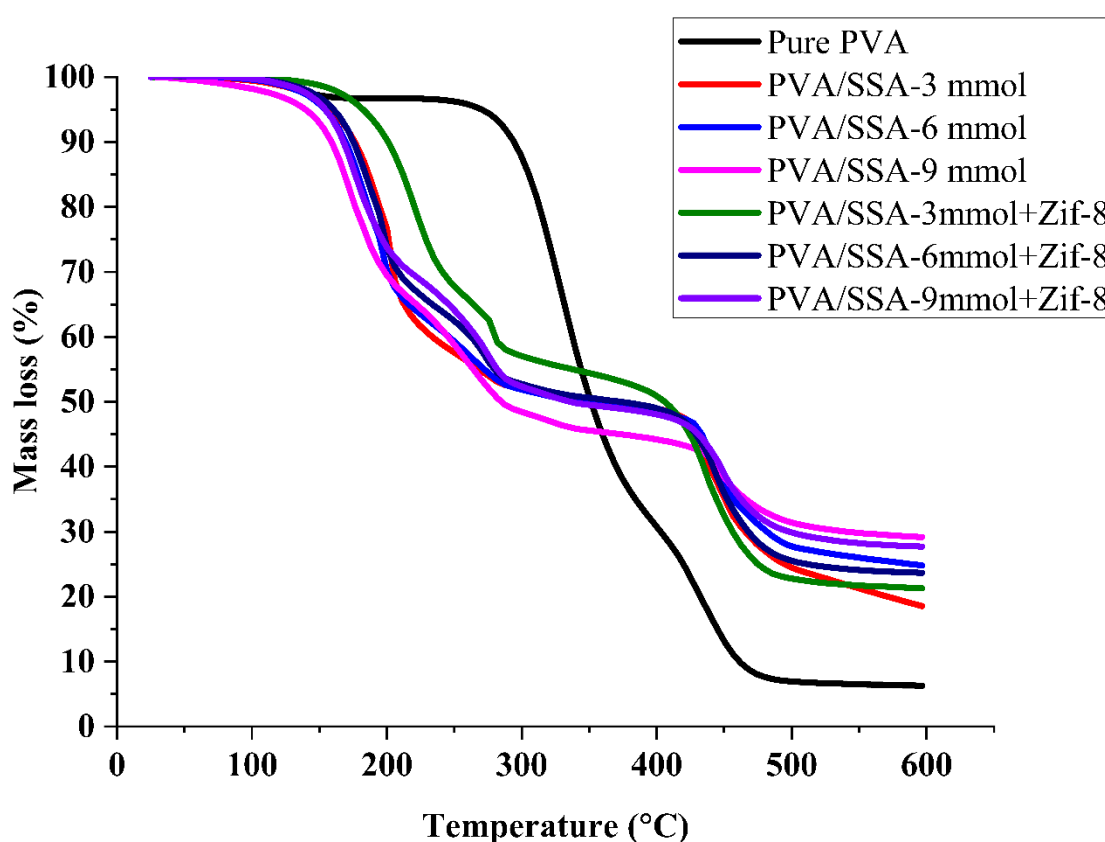
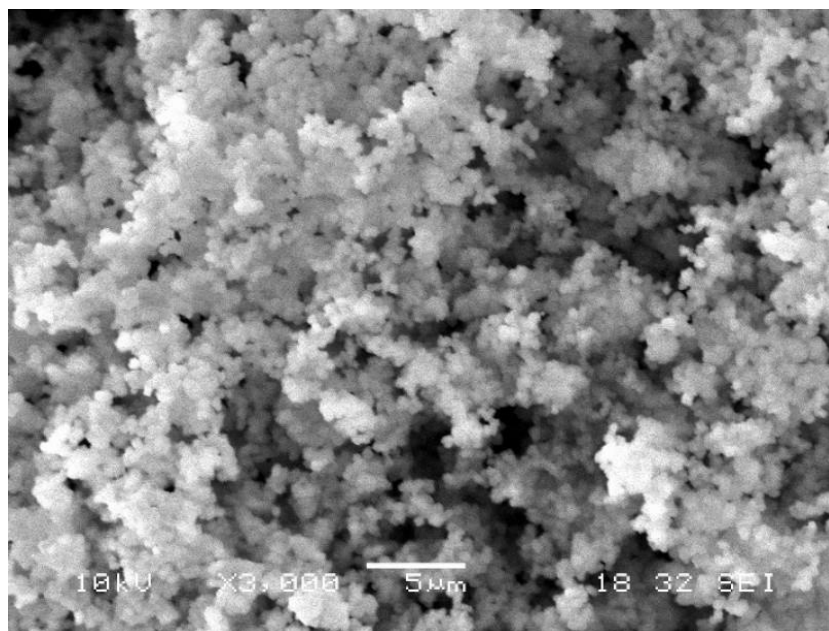


Fig. 4 TGA of PVA/SSA and PVA/SSA/ZIF-8 catalytic membranes

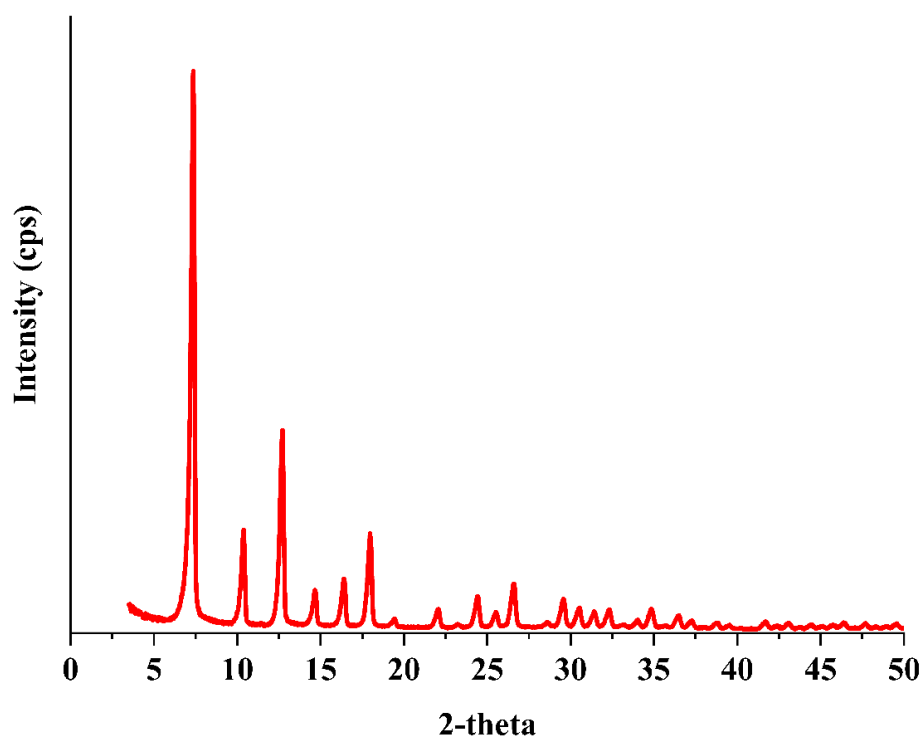
3.3. Scanning Electron Microscopy (SEM) and X-Ray Diffraction Analysis (XRD) Analyses of Synthesized ZIF-8

SEM image of the produced ZIF-8 is shown in Fig. 5. The SEM image of ZIF-8 is similar to the images in other studies in the literature (Attwa et al., 2024). The morphology of ZIF-8 contains

181 spherical ZIF-8 crystals (Thi Thanh et al., 2017). XRD peaks of produced ZIF-8 are shown in Fig. 6.
182 The high-intensity diffraction peak at $2\theta = 7.36$ is an important characteristic peak of ZIF-8, indicating
183 its high crystallinity (Qiu et al., 2022; Thi Thanh et al., 2017; Nordin et al., 2017).



184
185 **Fig.5 SEM image of ZIF-8 Crystals**
186



187
188 **Fig. 6 XRD of ZIF-8**

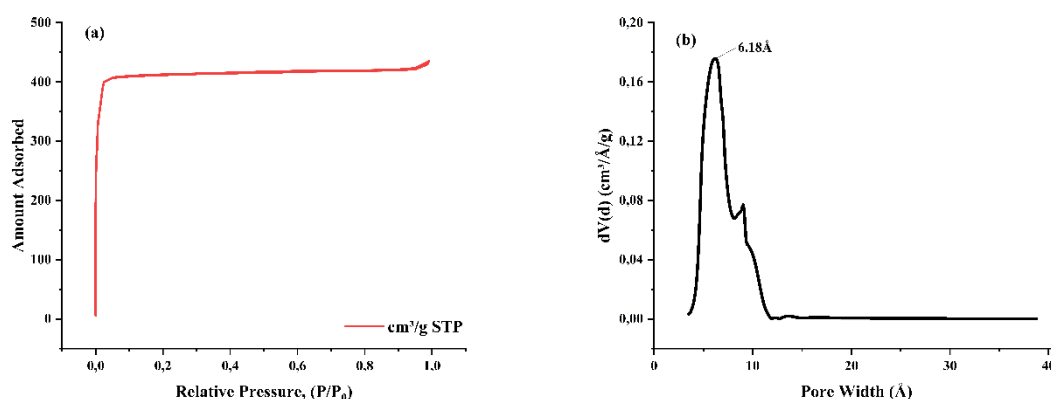
189 3.4. BET Analysis of ZIF-8

190 Table 1 shows the results of the BET analysis of ZIF-8.

191 **Table 1.** N₂ Adsorption/Desorption Data for the MOF of ZIF-8

<i>Adsorbent (MOF ZIF-8)</i>	
<i>S_{BET} (m²/g)</i>	1831.70
<i>Total Pore Volume (V_p (cm³/g))</i>	0.67
<i>Average Pore Size (Å)</i>	14.55
<i>BJH Adsorption Pore Diameter (Å)</i>	49.54
<i>BJH Desorption Pore Diameter ()</i>	38.93
<i>HK Method Pore Diameter (Å)</i>	4.32
<i>SF Method Pore Diameter (Å)</i>	6.18

192



193

194 **Fig. 7** (a) N₂ Adsorption/Desorption Isotherms Data for ZIF-8; (b) Pore Width(Å) for ZIF-8

195

196 Fig. 7 shows that ZIF-8 exhibits Type I isotherms according to the IUPAC classification. A significant
 197 increase in the amount adsorbed was observed at low P/P₀ values (0.015 P/P₀ 0.1). This result is
 198 typical for solid materials with microporous structures such as ZIF-8. According to the BET analysis,
 199 the specific surface area is 1831 m²/g, the total pore volume at P/P₀ = 0.99 is 0.66 cm³/g, and the pore
 200 size has a peak at 6.18 Å. Considering the range of 6.18 Å , where the peak is strongly observed, the
 201 pore size distribution shows that the material has a largely microporous structure. (Kruk and Jaroniec,
 202 2001; Pan et. al.,2011; Missaoui et. al.,2022; Zhang et. al.,2022)

203

3.5. Swelling Tests of PVA/SSA and PVA/SSA/ZIF-8 Catalytic Membranes

Swelling tests are performed to determine the affinity of a material for its solvent or reactants and products, if the material is to be used in a reaction medium. In this study, the synthesis of SoLE is an esterification reaction that releases water as a by-product. The presence of water in the reaction environment causes the reaction equilibrium to be directed to the side of the reactants, reducing the reaction yield. It is possible to shift the reaction towards product formation (Le Chatelier's Principle) by continuously removing water from the reaction medium (Liu and Ma, 2024; Zhu Jie et al., 2024). Therefore, the functional catalytic membrane must be hydrophilic. The water swelling results for the pure PVA, PVA/SSA, and PVA/SSA/ZIF-8 functional catalytic membranes used in the reaction are given in Tables 2 and 3. Water swelling rates were calculated with Equation (2).

$$\text{Swelling}(\%) = \frac{W_{\text{wet}} - W_{\text{dry}}}{W_{\text{dry}}} \times 100 \quad (2)$$

In Equation 2; W_{wet} and W_{dry} signify wet catalytic membrane weight (g) and dry catalytic membrane weight (g), successively.

Table 2 Swelling tests of PVA/SSA catalytic membranes

Catalytic membrane	Swelling Rate (%)
Pure PVA	755.2
PVA/SSA-3 mmol	401.3
PVA/SSA-6 mmol	499.4
PVA/SSA-9 mmol	553.8

Table 2 shows that when SSA was added to PVA, the swelling rate decreased compared to pure PVA. The heat treatment after the addition of SSA reduced the swelling rate by cross-linking. As the amount of SSA in the catalytic membrane increased, the swelling ratios rose due to the increased number of hydrophilic sulfonic acid groups (Yagizatli et al., 2022). In Table 3, when ZIF-8 was added to the

PVA/SSA catalytic membrane structure, a decrease in the swelling ratio was observed due to the hydrophobic effect of ZIF-8. (Sann et al., 2018).

Table 3 Swelling tests PVA/SSA/ZIF-8 catalytic membranes

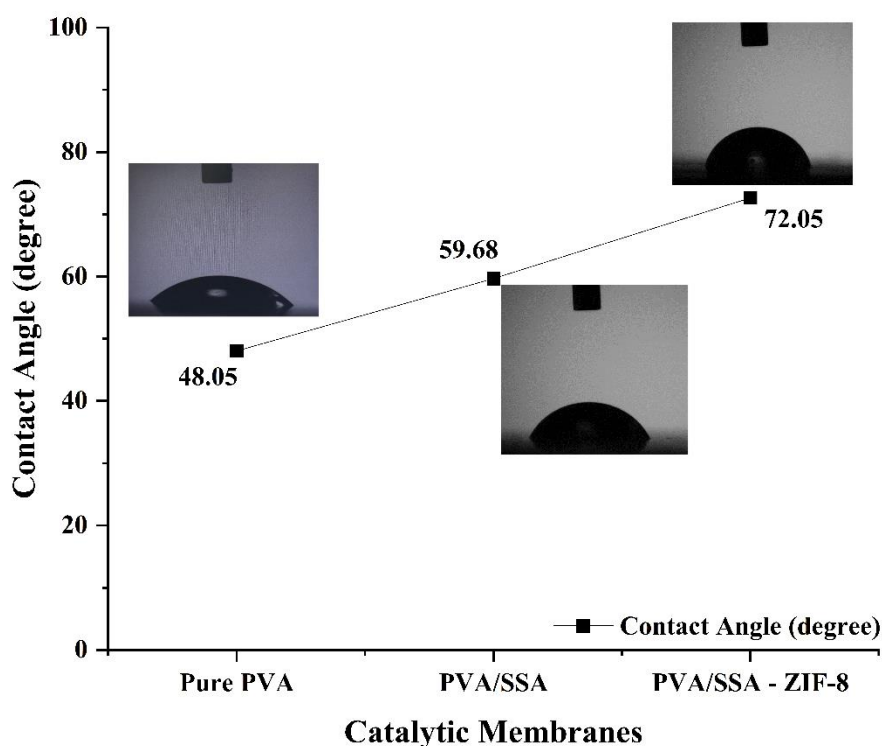
Catalytic membrane	Swelling Rate (%)
Pure PVA	755.2
PVA/SSA-3 mmol+ZIF-8	381.5
PVA/SSA-6 mmol+ZIF-8	419.7
PVA/SSA-9 mmol+ZIF-8	483.1

3.6. Contact Angle Testing

In this study, esterification reaction was carried out with solketal and levulinic acid as reactants and solketal levulinate was obtained as product. However, the accumulation of water as a by-product in the reaction medium will reduce the product yield/reaction conversion and needs to be removed. Therefore, for the preparation of the catalytic membrane used in the reaction, PVA polymer, which is highly hydrophilic, thermally and chemically stable and environmentally friendly thanks to the hydroxyl groups it contains, was chosen; hydrophilicity or hydrophobicity in a material is explained as the ability of the selected material to bind to water molecules with hydrogen bonds on the part of its surface in contact with water ((Li W. et. al., 2013; Rezaee et. al., 2015; Yadav D. et. al., 2022). Water was used in the contact angle test to understand the hydrophilicity of the prepared membranes. When the liquid makes an angle of less than 90° with the contact surface, it indicates hydrophilicity, while an angle of more than 90° indicates hydrophobicity (Milne A. J. B. and Amirfazli A., 2009).

Zeolitic imidazolate frameworks (ZIFs), a subfamily of MOFs, are materials with the ability to tune their pore size and high chemical functionality while ZIF-8s are a new type with zeolite topology and have excellent chemical stability and high structural diversity found in all zeolite varieties. Its high chemical properties and thermally stable behavior indicate that it can be easily recycled from its

243 environment in the process of use. ZIF-8 has a large surface area, strong and high degree of
 244 hydrophobicity (145°) and superoleophilic properties(San E. E. et. al.,2018; Zhang K. et. al.,2013).
 245 Hydrophobicity/Hydrophilicity property is shown in Fig. 8 with contact angle values.



246
 247 **Fig 8. Contact Angles Degree of Pure PVA, PVA/SSA and PVA/SSA – ZIF-8**

248 The addition of ZIF-8, which has high hydrophobicity, to the prepared PVA-based catalytic membrane
 249 brought the PVA polymer, which has high hydrophilicity, closer to its hydrophobicity. It is predicted
 250 that this gain in the catalytic membrane will provide energy efficiency by reducing the reaction time.

251 3.7. Interaction Parameters of PVA/SSA Catalytic membranes

252 The interaction between the by-product water and the polymer matrix of the catalytic membrane is
 253 well explained by the Flory-Huggins interaction parameter calculations. The Flory-Huggins
 254 interaction parameter helps to explain the interaction between a solvent and a polymer, based the
 255 amount of liquid sorbed by the polymer. As the interaction parameter approaches zero, the affinity of

the polymer for the solvent increases (Nistane et al., 2022). The interaction parameters for each SSA amount were calculated by Equations 3, 4, and 5.

$$\Phi_s = \frac{\frac{Q}{\rho_s}}{\frac{Q}{\rho_s} + \frac{1}{\rho_p}} \quad (3)$$

$$\Phi_p = 1 - \Phi_s \quad (4)$$

$$X_{ip} = - \frac{\ln(1 - \Phi_p) + \Phi_p}{\Phi_p^2} \quad (5)$$

Here, X_{ip} is the interaction parameter and dimensionless; Q (g/g) is the weight of water sorbed by one gram of polymeric membrane; ρ_s (g/cm³) and ρ_p (g/cm³) are densities of water and polymer, respectively. Φ_p and Φ_s are volume fractions of polymer and water, respectively. (Huang, 1991). The interaction parameters calculated for PVA/SSA catalytic membranes are shown in Table 4. A decrease in the values of the interaction parameters was observed as a result of increasing hydrophilicity with increasing number of hydrophilic sulfonic acid groups (Hasirci et al., 2023; Ohtake et al., 2022).

Table 4 Interaction parameters of PVA/SSA catalytic membranes

Catalytic membrane	Interaction parameter
PVA/SSA-3 mmol	0.521
PVA/SSA-6 mmol	0.486
PVA/SSA-9 mmol	0.439

3.8. Acidity of PVA/SSA and PVA/SSA - ZIF-8 Catalytic Membranes

The acidic or basic properties of catalysts can be explained by the amount of H^+ / OH^- ions in their chemical structure. Although there are different methods in the literature, the most widely used method for determining the amount of acid/base is the ion displacement reaction.

Ion displacement reaction is determined by classical acid-base titration to determine the degree of acidity of a material depending on the acid groups it has. This is done as follows; a certain amount of the material whose acidity is to be determined is taken and kept in 1M NaCl solution for 48 hours. The H^+ ions, which are replaced by Na^+ ions in the salt solution, are titrated with 0.05 M NaOH together with phenolphthalein, which is prepared before titration and acts as an indicator (Atkar A. et al.,2024). Ion exchange capacity is calculated by Equation 6:

$$IDR (mmol H^+ g^{-1}) = \frac{Consumption NaOH (ml) \times NaOH Molarite}{Sample Weight} \quad (6)$$

Calculated ion displacements are given in Table 5.

Table 5. Acidity of PVA/SSA and PVA/SSA - ZIF-8 Catalytic Membranes

ACIDITY (mmol H^+ g ⁻¹)	
PVA - (w/w) 3mmol SSA	15.23
PVA - (w/w) 6mmol SSA	>16
PVA - (w/w) 9mmol SSA	>18
PVA - (w/w) 3mmol SSA/ZIF-8	15.24
PVA - (w/w) 6mmol SSA/ZIF-8	>16
PVA - (w/w) 9mmol SSA/ZIF-8	>18

Acidity values were also given in Fig. 9.

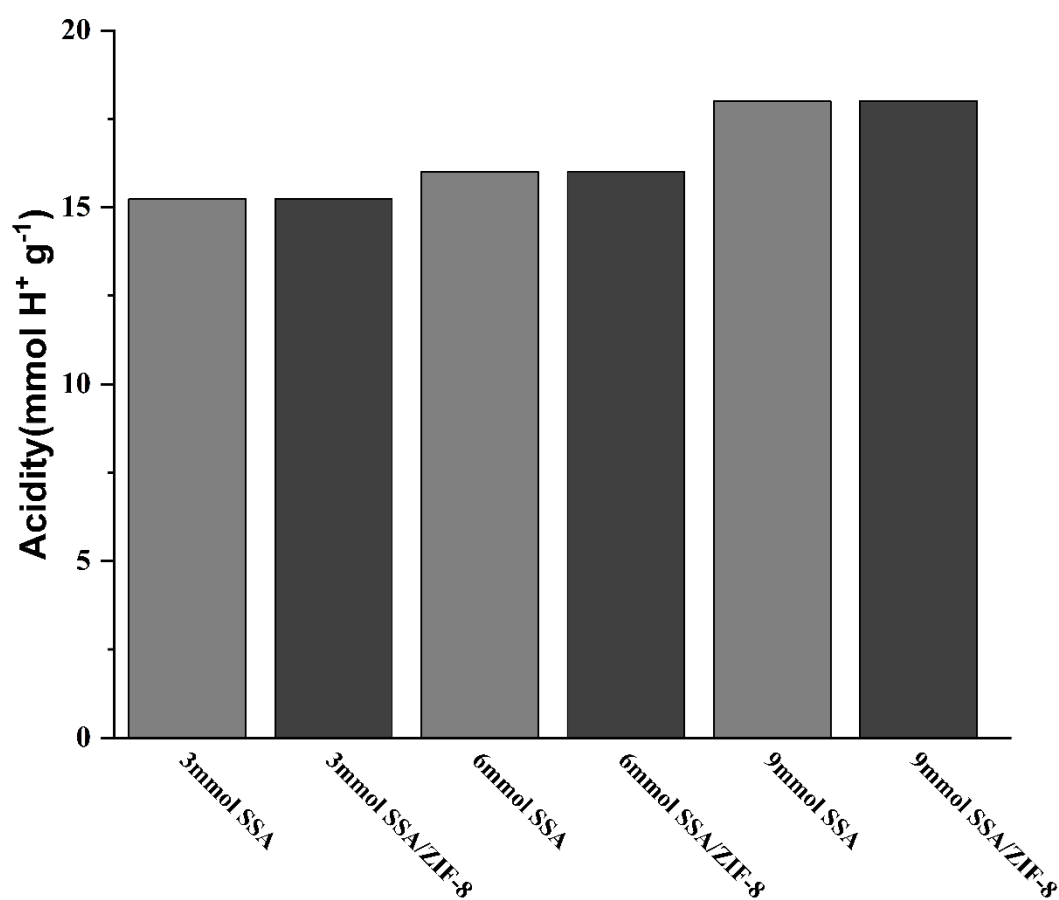


Fig 9. Acidity of PVA/SSA and PVA/SSA - ZIF-8 Catalytic Membranes

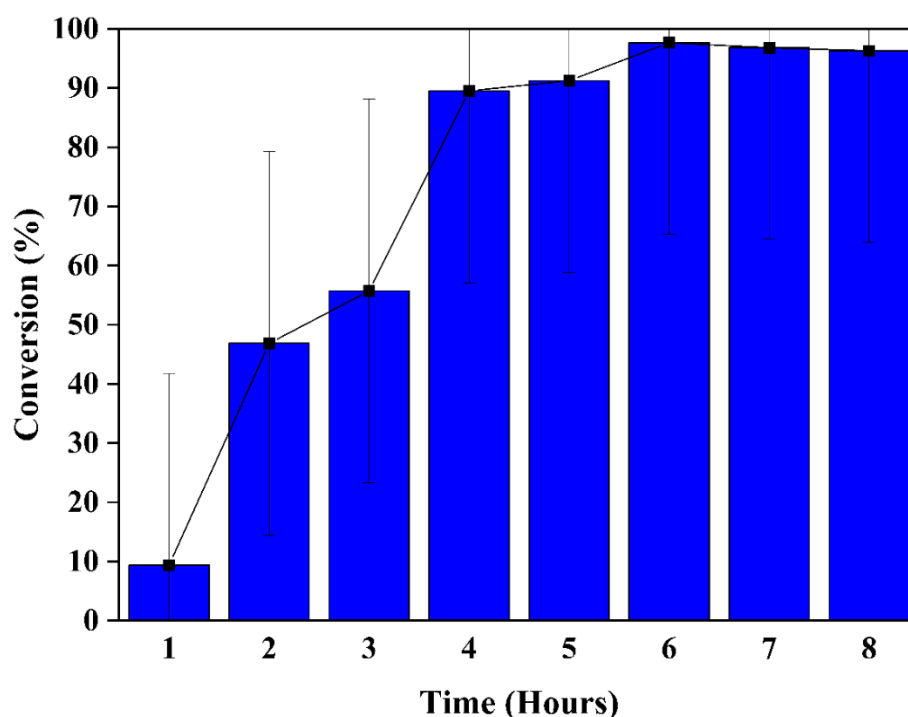
3.9. Batch Reactions with PVA/SSA and PVA/SSA/ZIF-8 Catalytic Membranes

Batch reactions with PVA/SSA and PVA/SSA/ZIF-8 catalytic membranes were performed at 105 °C and 3, 6, and 9 mmol SSA loadings, with Solketal/LA: 4/1, 5/1, 6/1 molar ratios. The effect of reaction time, SSA loading, and Solketal/LA ratio on reaction conversion was examined in batch reactions.

3.9.1 Influence of the reaction time on LA conversion

The influence of reaction time on the reaction conversion in the SoLE synthesis with PVA/SSA catalytic membranes at 9 mmol catalyst loading, with Solketal/LA: 6/1, and a reaction temperature of 105°C is given in Fig. 10. In the reaction carried out over the course of 8 hours, the conversion increased from 9.39% in the 1st hour to 97.65% in the 6th hour, where it reached a maximum. After

303 6 hours, small decreases in reaction conversion were observed. Since the SoLE synthesis is a
 304 reversible reaction, after the 6th hour, the reaction may begin to favor the reactants' side due to the
 305 increasing amount of water as a by-product. Therefore, the optimum reaction time was determined to
 306 be 6 hours. (Chansorn et al., 2022; Zhang et al., 2021; Zhu Jishen et al., 2024).



307

308 **Fig 10.** Influence of the reaction time on conversion with PVA/SSA catalytic membranes

309 To determine the optimized reaction time, SoLE synthesis was carried out with ZIF-8 doped
 310 PVA/SSA catalytic membranes at 9 mmol SSA loading, M:6/1 ratio, and 105 °C. As shown in Fig.
 311 11, the reaction conversion increased from 38.01% at 1 hour to 96.81% at 4 hours. After 4 hours, no
 312 significant change in reaction conversion was observed. After 4 hours, the reaction reached an
 313 equilibrium state, and there was no significant change in conversion. The hydrophobicity of ZIF-8
 314 prevented the occurrence of the reverse reaction. (Cao et al., 2021; Li et al., 2023). The optimum
 315 reaction time was determined to be 4 hours. The addition of ZIF-8 reduced the reaction time.

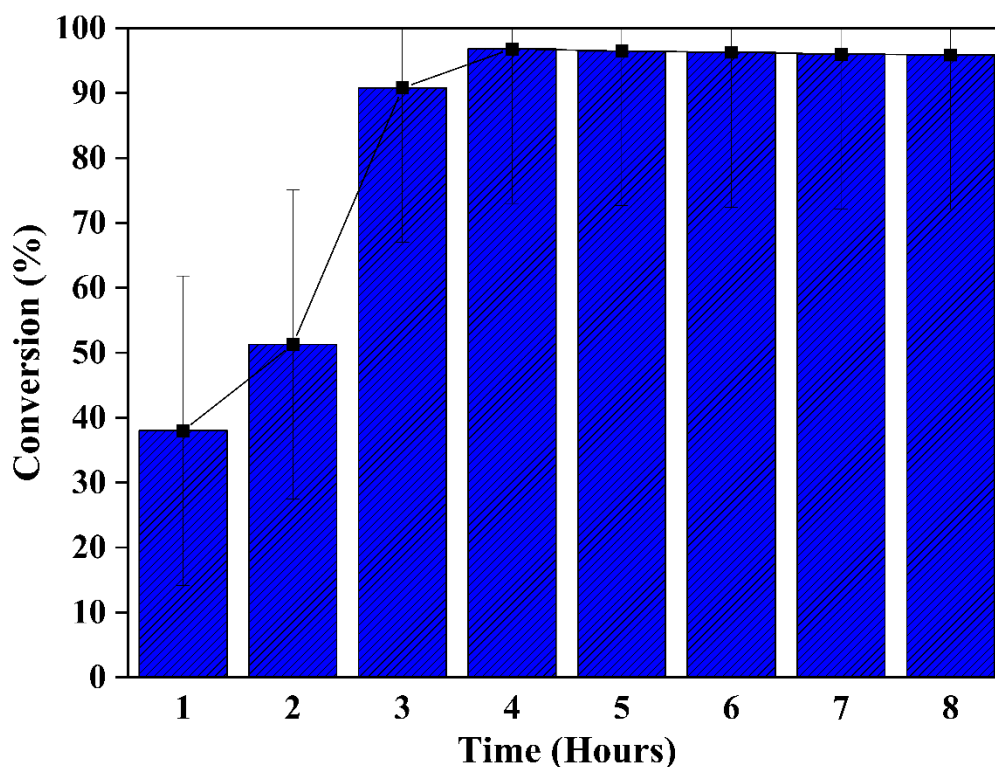


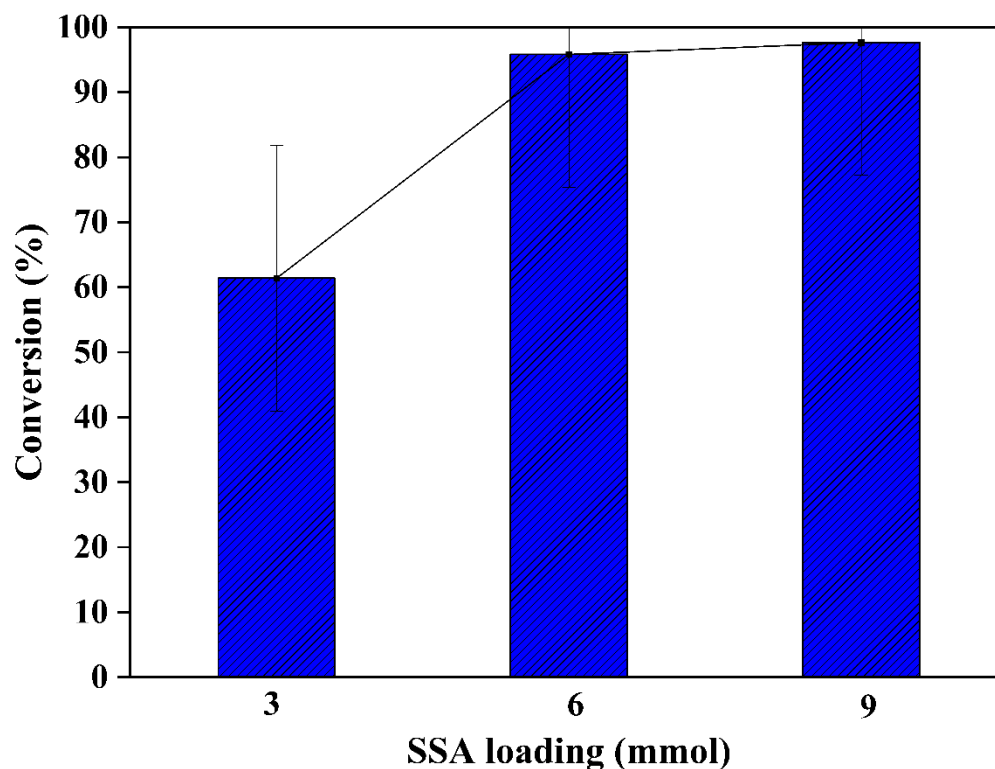
Fig 11. Influence of the reaction time on conversion with PVA/SSA/ZIF-8 catalytic membranes

Hydrophobic catalysts show high resistance to water. Since esterification reactions are reversible and limited by thermodynamic equilibrium, the hydrophobicity of the catalysts to be used allows the reacting organic molecules to adhere to the catalyst surface, while the desorption of by-product water molecules in esterification reactions and the selection of reactants in the reaction medium accelerate the reaction in the direction of the entrants and accelerate the ester formation (Liu, J. et. al., 2022). For this reason, they are often preferred for their ability to provide favorable conditions for reactants in esterification reactions. (Ristiana D. D. et. al., 2022; Suryandari A. S. et. al., 2023)

3.9.2 Influence of SSA loading on LA Conversion

The effect of SSA loading in the PVA/SSA catalytic membrane on LA conversion at 105°C and a 6/1 Solketal/LA ratio for 6 hours is presented in Fig. 12. The reaction conversion increased from 61.39% at 3 mmol SSA loading to 97.65% at 9 mmol SSA loading. Since the number of catalytically active sites in the membrane increased with increasing catalyst loading, an enhancement in reaction

330 conversion was observed (Zhang et al., 2024; Goda et al., 2022). However, a minimal difference was
331 observed in terms of reaction conversion at 6 mmol and 9 mmol SSA loading.



332

333 **Fig. 12** Influence of SSA loading on conversion with PVA/SSA catalytic membranes

334 At 105 °C and with a ratio of M to 6/1, reactions were performed for 4 hours to observe the effect of
335 the amount of catalyst on the reaction conversion in ZIF-8 doped PVA/SSA membrane. Fig. 13 shows
336 that while 8.75% conversion was obtained at 3 mmol SSA catalyst loading, dramatic increases to
337 conversion rates of 95.06% and 96.81% were obtained when the amount of catalyst was raised to 6
338 mmol and 9 mmol, respectively. No significant increase in reaction conversion was observed when
339 SSA loading was raised from 6 mmol to 9 mmol (Soltani et al., 2021; Al-Saadi et al., 2020).

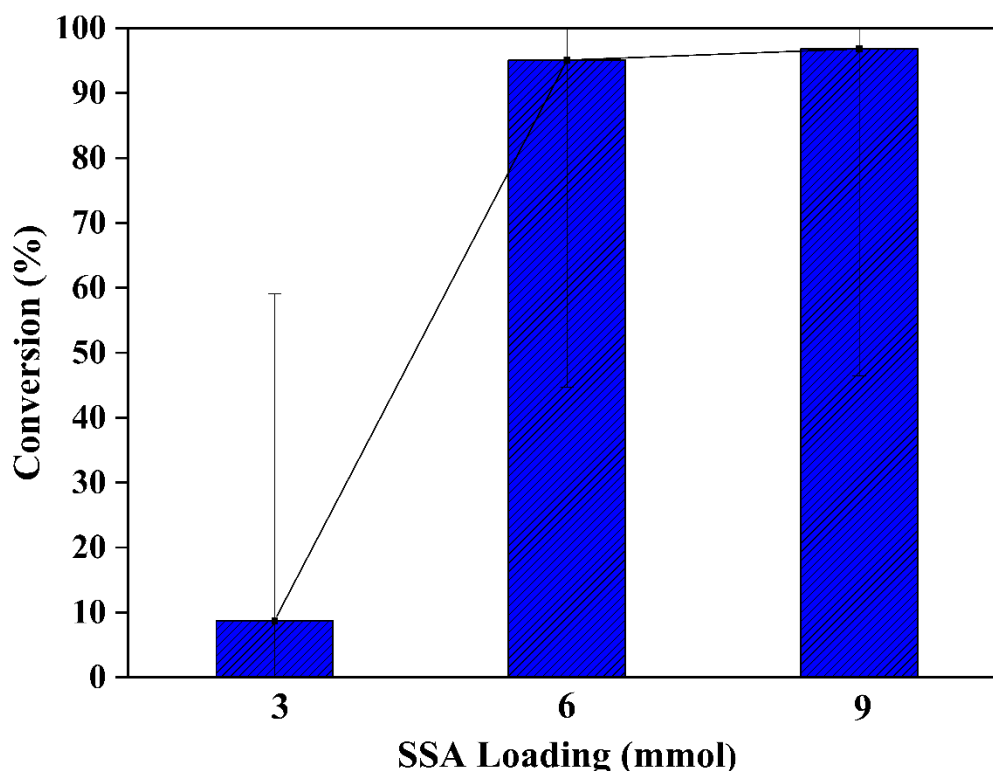


Fig. 13 Influence of SSA loading on conversion with PVA/SSA/ZIF-8 catalytic membranes

3.9.3 Influence of Solketal/LA initial molar ratio

To observe the effect of Solketal/LA molar ratio on the conversion with PVA/SSA catalytic membranes, the reactions were carried out at 105°C at a catalyst loading of 9 mmol for 6 hours, as shown in Fig. 14. At the molar ratios examined, very high conversions were obtained with very small differences in yields. While 95.26% conversion was obtained at M 4 to 1 ratio, conversion reached 97.65% at M 6 to 1 ratio. In the synthesis of SoLE (a reversible esterification reaction), feeding excess solketal, into the reaction medium can increase reaction conversion by shifting the balance towards product formation (Guo et al., 2021). However, the concentrations of the reactants and the conversion of the reaction may decrease due to the increasing amount of water, leading to a back reaction. (Cao et al., 2021). Thus, for the given molar ratios, increasing the Solketal/LA molar ratio did not cause a significant increase in the reaction conversion. The optimum molar ratio was determined as 4:1.

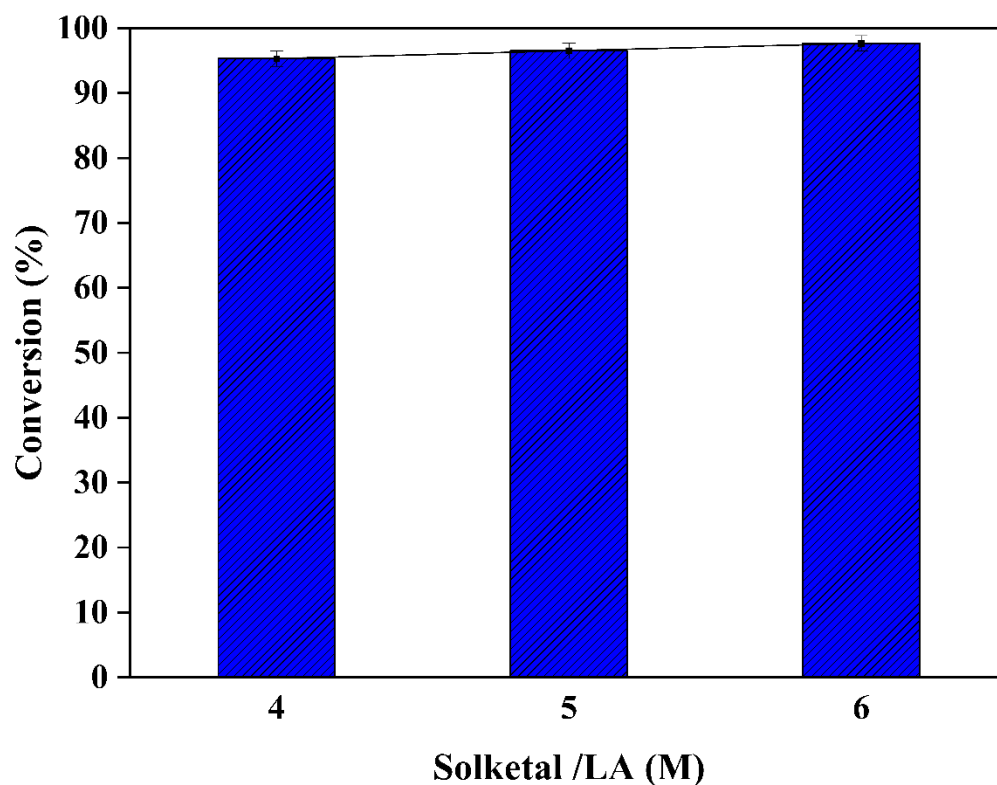


Fig. 14 Influence of Solketal/LA molar ratio on conversion with PVA/SSA catalytic membranes

The effect of Solketal/LA molar ratios of 4/1, 5/1, and 6/1 on reaction conversion with PVA/SSA/ZIF-8 catalytic membranes is shown in Fig. 15. The conditions of observation are 9 mmol catalyst loading, a 105 °C reaction temperature, and a 4 h reaction time. The reaction conversion was 93.97% at M:4/1, and reached 96.81% at M:6/1. The conversion data of the three different ratios were obtained very close to each other, as shown in Fig. 12. At the given molar ratios, the reaction conversion has reached the limit point (Mao et al., 2020). It was observed that the change in the determined molar ratios did not significantly affect reaction conversion.

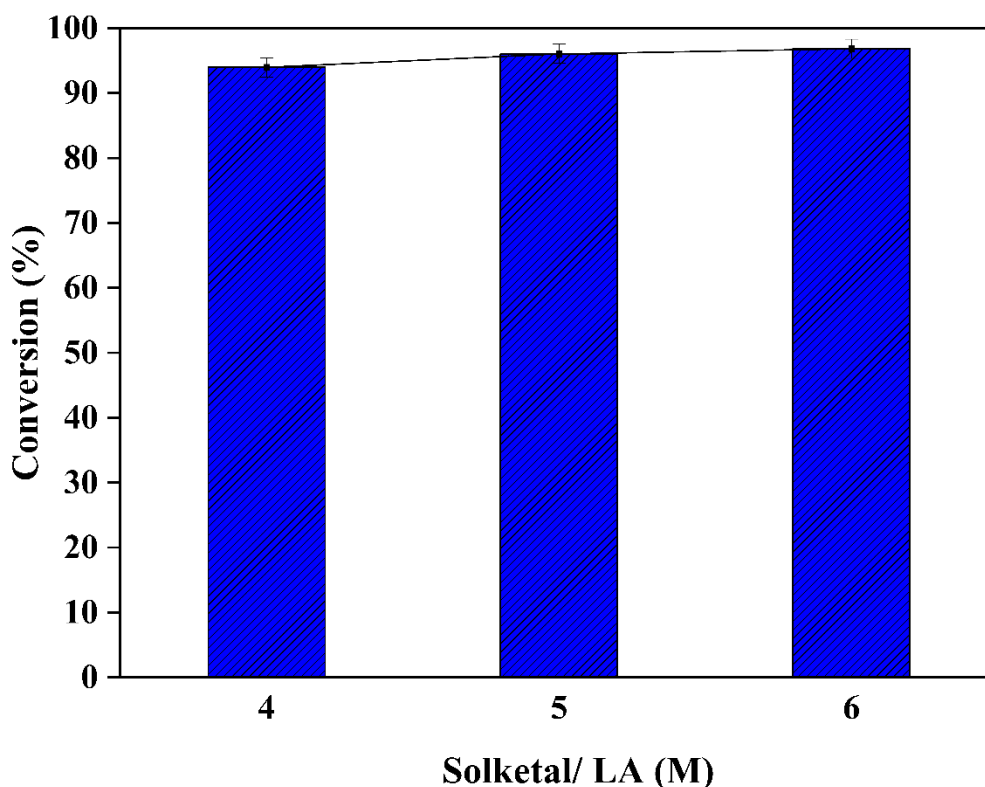


Fig. 15 Influence of Solketal/LA molar ratio on conversion with PVA/SSA/ZIF-8 catalytic membranes

4. Conclusions

In this study, a new generation of environmentally friendly fuel additive, solketal levulinate, was synthesized from the esterification of solketal and levulinic acid using functional PVA/SSA and PVA/SSA/ZIF-8 catalytic membranes in a batch reactor under mild conditions for the first time in the literature. Functional catalytic membranes were produced from a PVA matrix, SSA as a catalyst, and ZIF-8, a type of MOF, as a support material. The peak (S-O bond) at 1035 cm^{-1} in the FTIR analysis of the produced catalytic PVA/SSA membranes confirms the SSA loading. In addition, the presence of ZIF-8 in the PVA/SSA/ZIF-8 catalytic membrane structure increased the hydrophobicity of the structure. In TGA analysis, the integration of SSA to the PVA matrix increased the thermal stability. In swelling tests in water, SSA increased the hydrophilicity of the structure by increasing the extent of swelling. The catalytic membrane's ability to absorb water increases with an increasing swelling rate, thereby increasing the sorption support. The increased hydrophilicity of the catalytic membrane

with increasing SSA was supported by interaction parameter values approaching zero. The image of synthesized ZIF-8 crystals obtained by SEM was consistent with the literature. The high crystallinity of ZIF-8 crystals was determined by XRD analysis. The LA conversion obtained in SoLE production with a PVA/SSA functional catalytic membrane at 9 mmol catalyst loading, 105 °C, Solketal/LA molar ratio of 6/1, and a reaction time of 6 hours was **97.65%**, while the reaction conversion was 96.81% in SoLE synthesis with a PVA/SSA/ZIF-8 catalytic membrane under the same catalyst loading, temperature, and molar ratio, but with a reaction time of 4 hours. In this reaction, MOF ZIF-8 significantly reduced the reaction time, an improvement that cannot be ignored in terms of system cost. The developed functional catalytic membranes are promising and effective materials for the potential fuel additive SoLE synthesis.

Statements And Declarations

Competing Interests: The authors declare no conflict of interest.

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