

# Copper recovery by slurry electrolysis using ionic liquids from waste printed circuit boards

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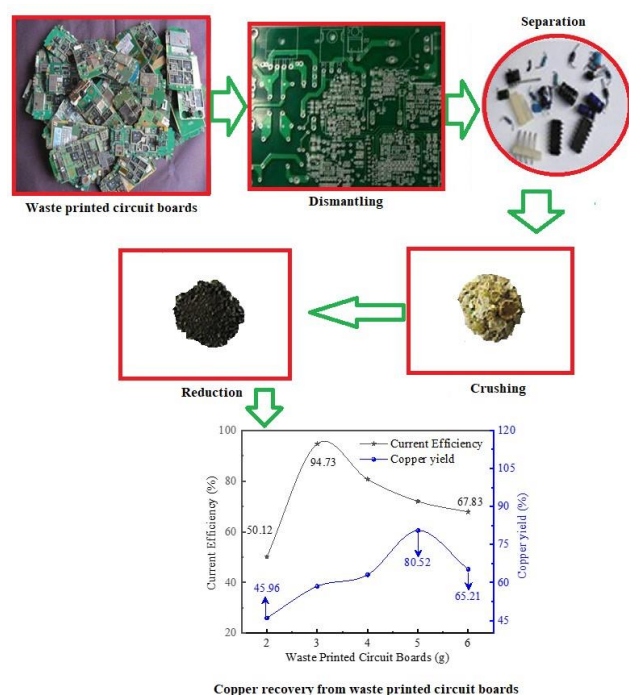
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## Graphical abstract



## Abstract

The regulatory framework of heavy metal pollution associated with electronic waste is prevalent all over the world. As a result of technological advancement and change in consumer patterns, the life span of electrical and electronic products has been shortened. This has contributed to the emergence of massive amounts of electronic waste that needs to be handled. With the exponential growth of the telecommunications sector, the recycling of useful resources from electronic waste devices, especially mobile phones, is of great significance. Besides, the presence of valuable metals enables the recycling of electronic waste potentially appealing. In this research, numerous types of ionic liquids like Butyl

methylimidazolium hexafluorophosphate [Bmim][PF<sub>6</sub>], Butyl methylimidazolium chloride [Bmim][Cl], Ethyl methylimidazolium chloride [Emim][Cl] and Butyl methylimidazolium tetrafluoroborate [Bmim][BF<sub>4</sub>] were used to analyze the copper leaching behavior of electronic mobile handset devices. Several influential aspects on the leaching efficiency of copper including different types of ionic liquid, temperature and leaching time have been examined. The findings showed [Bmim][PF<sub>6</sub>] and [Emim][Cl] were better ionic liquids in appropriate conditions for high copper leaching rates.

**Keywords:** copper metal leaching, different ionic liquids, electronic waste, slurry electrolysis

## 1. Introduction

As a conventional electronic waste, the abundant production of cell phone waste in recent years has demonstrated that it is highly essential to recycle useful materials from mobile phone waste and in the meantime to monitor the emission of dangerous materials (Sarwar *et al.*, 2020; Qiu *et al.*, 2020). Effective disposal and recycling of electronic waste are of great significance for the adaptive re-use of useful materials including precious metals, zinc, copper, etc. and for eliminating emissions of hazardous components like lead and cadmium (Delcea *et al.*, 2020). Printed circuit boards include numerous procurement metals as gold, platinum, etc and base metals such as copper, aluminum and so on as the key frames of electronic devices (Miner *et al.*, 2020; Holgersson *et al.*, 2018). Consequently, effective manufacturing of waste printed circuit boards is an immediate requirement that promotes the recycling and re-use of useful materials (Adamo *et al.*, 2019).

Electrolysis treatment of waste printed circuit boards primarily focuses on the electrodeposition of metals, which reported in a few surveys and cases (Chu *et al.*, 2015). The complete removal of metals and non-metals from waste printed circuit boards was obtained by slurry

electrolysis. The metal and non-metal removal percentage achieved 97% with a copper recovery of almost 99% (Yang *et al.*, 2018).

Slurry electrolysis includes electrowinning, solvent purification, leaching, and electrodeposition in a single operation, consisting of cathodic (electrodeposition) and anodic (dissolution of metal) sections (Chu *et al.*, 2015). Effective recovery from CPU sockets of copper and gold by slurry electrolysis. Purity and recovery of copper were up to 98% and 96%, respectively (Li *et al.*, 2019).

Recovered high purity copper cathode using ammonia sulfate solution printed circuit boards (Sun *et al.*, 2015). Copper was eventually recovered from electrodeposition in the sulfate systems after leaching and solvent extraction. A simultaneous electro-leaching process carried out the direct copper recovery from the powder of waste printed circuit board. Apparent recovery of 96% of copper was achieved at 25 °C (Choubey *et al.*, 2015).

Ionic liquids (ILs) are usually based on cations and anions, which possess a low vapor pressure, thermal stability and broad electrochemical window, high conductivity, and wide range of liquid temperatures, non-volatilization, etc (Muhammad Tariq *et al.*, 2020; Singh and Savoy, 2020). A potential study was carried out to dissolve epoxy bromine resins with printed circuit boards using [EMIM+][BF<sub>4</sub>-] ionic liquid to recover copper foils and glass fibers. The full separating of waste printed circuit boards was obtained by processing copper and glass fibers at a 260 °C temperature (Zhu *et al.*, 2012). The leaching of copper tendencies were studied present in waste printed circuit boards by different ionic liquids and also optimum situations produced about 98% copper leaching efficiency (D. Zhang *et al.*, 2018). Also, the recovery output of metals has been tested with different types of ionic liquid and the results of numerous operating aspects have been calculated from waste printed circuit boards (Chen *et al.*, 2015; Gu *et al.*, 2019). Chemical reagent [BSO<sub>3</sub>HPy][HSO<sub>4</sub>] was used in slurry electrolysis process to extract copper from waste printed circuit boards. The optimum standard was achieved with a recovery rate, purity, current performance and copper powder particle size of 90%, 81%, 70%, and 2.30 μm (Y. Zhang *et al.*, 2018).

Despite some novel discoveries in the recovery of metals from waste printed circuit boards using ionic liquid, the processing of copper has not adequate using slurry electrolysis from waste phones. It is essential for effective recovery of copper to evaluate the appropriate kind of ionic liquids. This study therefore used waste mobile phones of similar form as a target entity for analysis and as leaching solvent used [Bmim][Cl], [Bmim][BF<sub>4</sub>], [Bmim][PF<sub>6</sub>], [Emim][Cl] ionic liquids. Different influential operating aspects on the performance of copper leaching including various types of ionic liquid, leaching time and temperature were analyzed.

## 2. Materials and methods

### 2.1. Materials and reagents

All major reagents such as HNO<sub>3</sub> chemical with purity AR,65.0-68.0%, HClO<sub>4</sub> chemical with purity AR,70.0-

72.0%, H<sub>2</sub>SO<sub>4</sub> purity AR,95.0-98.0%, HCl purity AR,36.0-38.0% were purchased from Shanghai Susong Chemical factory. CuSO<sub>4</sub>•5H<sub>2</sub>O, NaCl, H<sub>2</sub>O<sub>2</sub> and C<sub>6</sub>H<sub>5</sub>N<sub>3</sub> were purchased from Shanghai Guangnuo Chemical factory. C<sub>6</sub>H<sub>11</sub>ClN<sub>2</sub> chemical with purity AR,99% and C<sub>8</sub>H<sub>15</sub>ClN<sub>2</sub> chemical with purity AR,99% were purchased from Lanzhou Institute of Materialization factory. C<sub>8</sub>H<sub>15</sub>PF<sub>6</sub>N<sub>2</sub> with purity of AR,99% and C<sub>8</sub>H<sub>15</sub>BF<sub>4</sub>N<sub>2</sub> chemical with purity of AR,99% were purchased from the Shanghai Chengjie Chemical company. [Bmim][Cl], [Bmim][BF<sub>4</sub>], [Bmim][PF<sub>6</sub>] and [Emim][Cl] ionic liquids were used.

In order towards unify test conditions, 30Kg of same types of waste mobile phone circuit board materials were purchased in this study. Electric gears including USB ports, camera and microphone have been well separated from cell phone frames. Then, used cutting grinder to crushed well of waste boards upto the size of 0.9mm. The original waste printed circuit boards contained 89.89%, 1.91%, 6.74%, 1.07%, and 0.39% of copper, iron, zinc, platinum and aluminum.

### 2.2. Experimental procedure

In order to examine the influence of different factors on the performance of leaching of copper by using various types of ionic liquid, every kind of ionic liquid was used to prepare a specified solution quantity at certain temperatures. For (BmimPF<sub>6</sub>-Cu(PF<sub>6</sub>)<sub>2</sub>) ionic liquid solution preparation, first 5 ml ion liquid of [Bmim][PF<sub>6</sub>] was put in 5 beakers, respectively. Five beakers were put in the water bath and feed materials with a weight of 1 g, 2 g, 3 g, 4 g, and 5 g were fed into beakers with a 25°C temperature and 60 min of heating time. The plate was washed for 3 min with 13% concentration of hydrochloric acid (diluted) and was continually cleaned for further 10 min with alcohol (absolute). Plate was eventually clean rinsed and for further used oven dried it.

Copper recovery rate is calculated as shown in Eq. (1).

$$\text{Recovery Rate(\%)} = \frac{X}{X_1} \times 100 \quad (1)$$

Where  $X$  is the recovery amount in gram (g); the mass of the metal recovered after electrolysis reaction;  $X_1$  is the initial content of metal in waste printed circuit boards.

The current efficiency calculation method of copper is as shown in Eq. (2)

$$\eta_{\text{Cu}} = \frac{Y_1}{Y_2} \quad (2)$$

Where  $Y_1$  is the mass of copper obtained in the actual test in g;  $Y_2$  is the mass of copper theoretically calculated according to Faraday's law in g; The formula for calculating  $Y_2$  is in Eq. (3):

$$Y_2 = t \times K \times I \quad (3)$$

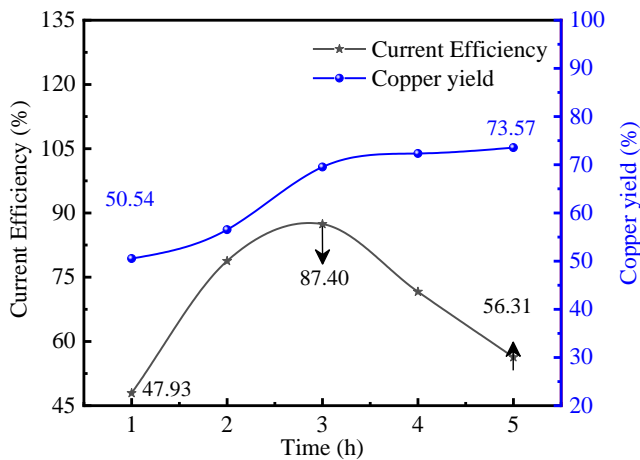
Where  $t$  is the time of energization (h);  $K$  is electrochemical coefficient (g/h\*A);  $I$  is the intensity of current (A); the value of copper electrochemical coefficient is 1.18 g/h\*A.

### 3. Results and discussion

#### 3.1. Influence of time on recovery rate of copper

It's visible from Figure 1 The copper recovery rate rises with the reaction time and there is no intervention point for the recovery of copper. So if the time varies from 1h to 5h, the copper recovery rate obviously changes from around 50% to 73%.

On the other hand, the current efficiency showed an inflection point during the entire reaction phase. When the time shifted from 1 to 3 hours, current productivity rose from around 47% to 87%. The current efficiency declined to around 56% percent as the reaction proceeded. Therefore the current efficiency achieved the optimum value when the reaction was conducted over 3 hours.



**Figure 1.** Influence of time on copper recovery and current efficiency

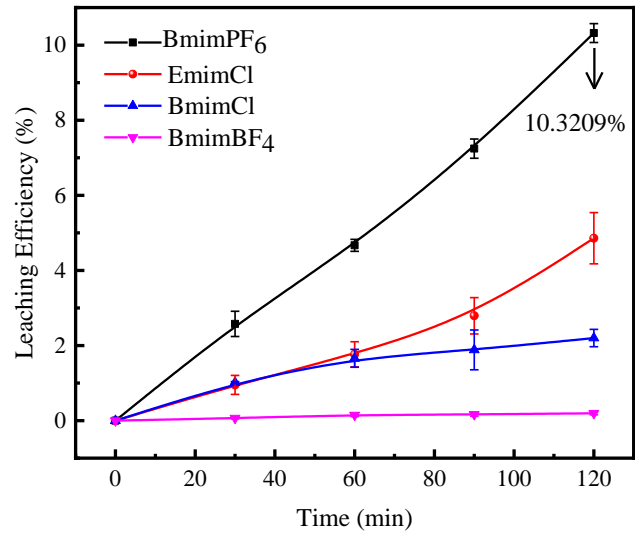
According to the study, the anode is quickly oxidized when the electrolysis process is just underway, and the reaction is intensive enough that a lot of metal is extinguished. Metal cation is continuously given for the entire anodizing phase for the reaction, so that the cathode decrease reaction is fast and the metal is deposited electrolytically in large amounts and the recovery speed becomes increase. As the reaction process continues, the anodyne reaction promotes metal laxation at a much slower rate than the cathode redox reaction, which supports side reactions mainly due to the apparent process of hydrogen transformation. Other metals are deposited together in the electrolyte copper metal, which affects metallic copper recovery and also reduces electrical energy utilization.

#### 3.2. Influence of ionic liquids

Leaching efficiency of copper influence by four different ionic liquids which is seen in Figure 2. The findings revealed that prevalence of pure copper leaching was effectively a linear increase of leaching time with different ionic liquids.

Generally, the most significant copper leaching influence level of Ionic liquids was (Bmim-BF<sub>4</sub>) < (Bmim-Cl) < (Emim-Cl) < (Bmim-PF<sub>6</sub>). Conclude, the overall leaching rate of copper 10.3209% was obtained with 50°C of leaching

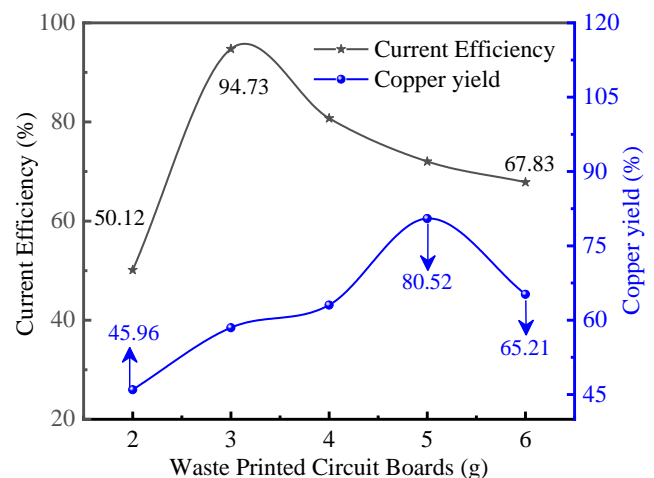
temperature and time of 120 min by using Bmim[PF<sub>6</sub>] as solution. Ionic liquids have a leaching effect on metallic copper because these four ionic liquids are an acidic liquid. As a new "Green Solvent," it has also been used in metal minerals to leach metals.



**Figure 2.** Influence of different ionic liquids on leaching of copper efficiency

#### 3.3. Influence of waste printed circuit boards dosage on copper recovery rate

Figure 3 indicates that during the test the highest inflection point occurs for the copper recovery rate. When the Waste Printed Circuit Boards feed volume is 5g, the recovery rate for copper exceeds 80%. With the feed rate continuing to grow, however, the recovery rate is reduced to 65% but copper relative recovery rate is 45%. The feedstock quantity remains a factor in improving the copper recovery rate. In comparison with the current efficiency, as the feed rate of Waste Printed Circuit Boards increases from 2g to 3g Copper real efficiency rises from 50%, to 94% but when the feeding rate of Waste Printed Circuit Boards continues to rise to 6g, its current efficiency declines up to 67%.

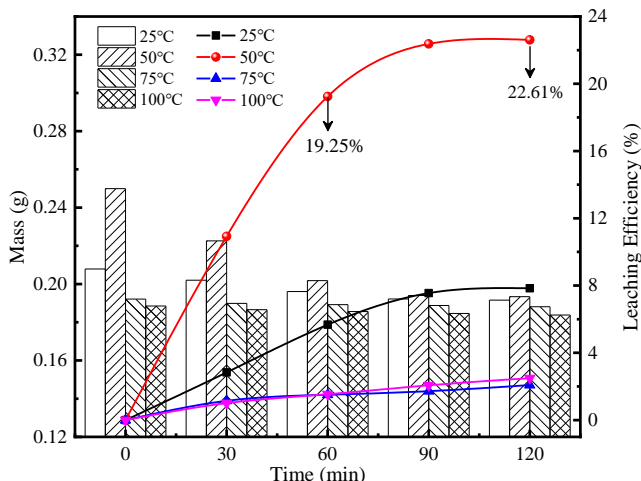


**Figure 3.** Influence of WPCBs dosage on copper recovery and current efficiency

The study suggested that the continued addition of Waste Printed Circuit Boards to the electrical process is not conducive when the feed rate for the Waste Printed Circuit Boards rises to a higher concentration. Although the copper content of the raw materials is increased, more mixture of metal or non-metallic impurities affects the electrolysis reaction simultaneously.

### 3.4. Influence of time and temperature on [Bmim][PF<sub>6</sub>] solution

As revealed in Figure 4, the copper leaching rate for the solution of ionic liquid [Bmim][PF<sub>6</sub>] and 50°C leaching temperature showed a remarkable rise with the increase of the leaching time. The copper leaching rate was relatively high around 19% and 22% for 60 minutes and 120 minutes respectively. In addition, the copper leaching rate also demonstrated a significant rise in the leaching duration at 25°C of leaching temperature. The growing trend, however, was less obvious than the 50°C temperature. The rate of copper leaching did not display any significant increase in the leaching cycle, if the leaching temperature increased to 100°C.



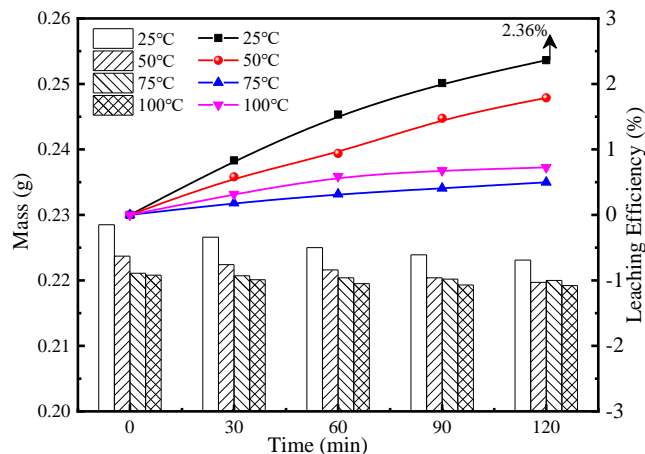
**Figure 4.** Influence of time and temperatures on copper leaching of BmimPF<sub>6</sub>

[Bmim][PF<sub>6</sub>] ionic liquid is highly oxidizable. The proper increase in the leaching temperature can boost [Bmim][PF<sub>6</sub>] oxidizability.

### 3.5. Influence of time and temperature on [Bmim][BF<sub>4</sub>] solution

As revealed in Figure 5, with [Bmim][BF<sub>4</sub>] solution at 25°C leaching temperature with rise in leaching time, the copper leaching rate steadily improved. In fact, the maximum copper leaching rate was reached at 25°C and 120 min. The leaching temperature was around 2%. However as the temperature for the leaching rose to 100°C, leaching rate of copper increased significantly.

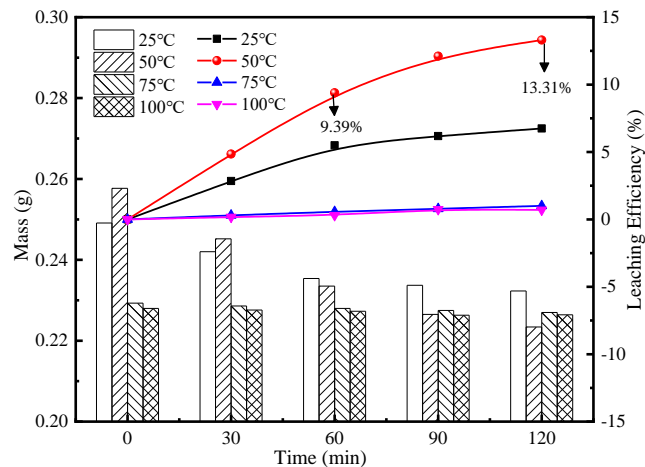
The high liquid temperature causes [Bmim][BF<sub>4</sub>] to react inactively as a solution. In addition, [Bmim][BF<sub>4</sub>] demonstrates solubility with water at average temperature. The mutual solubility of [Bmim][BF<sub>4</sub>] declines as the leaching temperature increases.



**Figure 5.** Influence of time and temperatures on copper leaching of BmimBF<sub>4</sub>

### 3.6. Influence of time and temperature on [Emim][Cl] solution

As seen in Figure 6, the leaching rate of copper increased steadily as time increased 0 to 60 minutes and at 25°C of leaching temperature on solution of [Emim][Cl] and appeared to be constant as the leaching period continued to increase. In comparison, leaching efficiency of copper enhanced dramatically by leaching interval at 50°C of leaching temperature. In addition, leaching rate of copper was around 9% and 13% percent for 60 minutes and 120 minutes. But as the leaching temperature rises to 100°C, the rate of leaching of copper did not rise considerably as the leaching time rose.

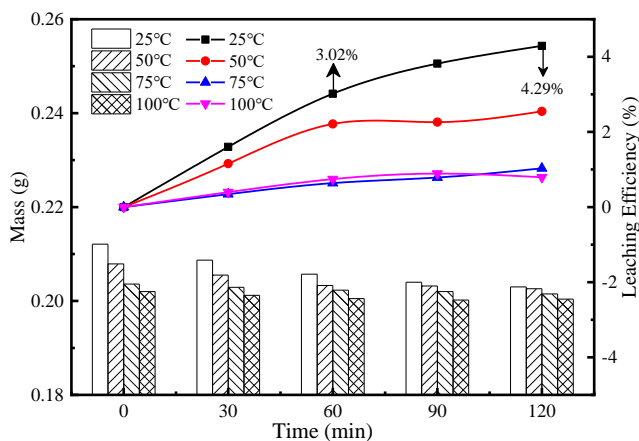


**Figure 6.** Influence of time and temperatures on copper leaching of EmimCl

The appropriate change of temperature can catalyze and endorse leaching reaction. Although it is difficult to mix oxygen produced by decomposing H<sub>2</sub>O<sub>2</sub> into ionic liquids when the leaching temperature is too high and then volatilize it out of reaction pot. Oxygen level therefore declines drastically in entire process (ionic liquid), which decreases leaching efficiency of copper and stands unfavorable towards copper oxidation. Briefly, ideal ionic liquid [Emim]Cl leaching temperature is 50°C with a 120 min of leaching rate.

### 3.7. Influence of time and temperature on [Bmim][Cl] solution

As seen in the Figure 7, at a leaching temperature of 25°C showed a clear rise as the leaching time increased on [Bmim][Cl] solution. The copper leaching rate in generally was around 3% and 4%, and the leaching interval was 60 minutes and 120 minutes. In comparison, the elevated copper leaching rate was not as noticeable at leaching temperature of 50°C compared with 25°C. Likewise, leaching efficiency of copper as leaching temperature rose to 100°C did not evidently rise as the leaching time increased.



**Figure 7.** Influence of time and temperatures on copper leaching of BmimCl

As the explanation for Figure 6 illustrated. Correspondingly, an appropriate leaching temperature is required as a solution for [Bmim][Cl].

### 3.8. Influence of current on copper recovery

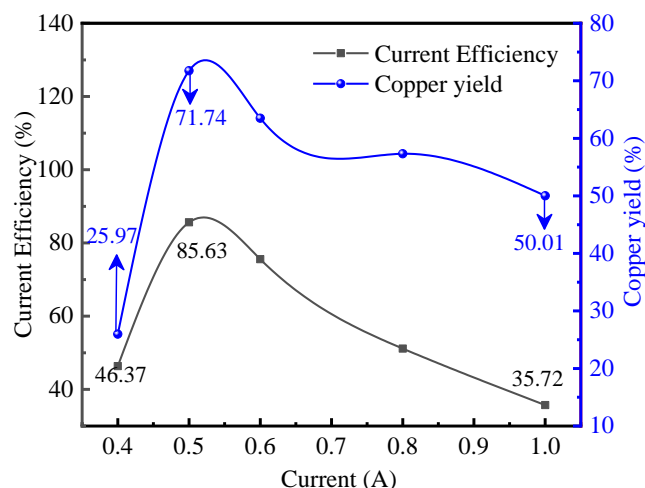
It's seen from Figure 6 that the inflection point occurs during the entire reaction phase for the copper recovery rate. Initially, electricity is increased and the copper recovery effect is evident. When the current is increased from 0.4A to 0.5A, the copper recovery has increased around from 25% to 71%. The amount of electricity increased continuously and the recovery rate of copper decreased to 50.01% at 1.0A. The recovery rate of copper was still improved in this time frame relative to the initial.

On the other hand, at the highest point of inflection, current efficiency reached about 85% while the current is 0.5A. Continue to boost the current level to 1.0A which results the reduction in current performance around 35%. The low current power 0.4A demonstrated a current efficiency of 46% and the current efficiency is not increased by the high electricity.

According to the low electricity calculation, a large number of useful electrons are increased at a lower current value. The current increase promotes the reaction, which increases the recovery rate of metal copper and the whole process.

However, if the amount of electricity continues to rise, the current is extended. The voltage corresponding to the entire electrolytic cell is also increased, thereby speeding up the electrolytic recovery of copper and facilitating

deposition. The solution's concentration is considerably reduced and the cations are essentially filled in the cathode chamber in the whole electrolyte, which results in more unsuccessful side reactions because of the hydrogen evolution reaction. Other metals will also deposit in the electrolyte along with the metal copper that affect the rate of recovery of metallic copper. It also decreases electrical energy usage in the electrolysis reaction.



**Figure 8.** Influence of current magnitude on copper recovery and current efficiency

### 3.9. Slurry electrolysis copper recovery with ionic liquid (BmimPF<sub>6</sub>)

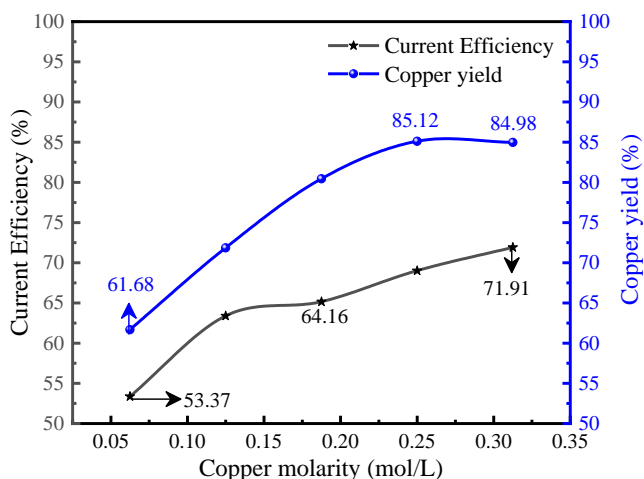
Table 1 displays the copper electrodeposition experimental parameters in BmimPF<sub>6</sub>-Cu(PF<sub>6</sub>)<sub>2</sub> ionic liquid solution.

**Table 1.** Copper electrodeposition experimental parameters

Current intensity (A)	Time (h)	Temperature (°C)	Copper molarity (mol/L)
0.5	10	25	0.08
0.5	10	25	0.15
0.5	10	25	0.19
0.5	10	25	0.23
0.5	10	25	0.32

Figure 9 shows influence of the copper molar concentration on the recovery of copper and ionic liquid solution of BmimPF<sub>6</sub>-Cu(PF<sub>6</sub>)<sub>2</sub> current efficiency. Recovery of copper rose from 61% to 85%, when copper molarity concentration enhanced 0.08-0.23 mol/L. With the copper molarity continuously rising upto 0.32 mol/L then copper recovery rate dropped at 84%. Similarly, current productivity improved from 53% to 64% as the molar copper concentration augmented 0.08-0.19 mol/L, which was eventually improved 71% as the incessant rise in the concentration of copper molarity to 0.32 mol/L.

Copper concentrations increase in solution of ionic liquid would rise current cathode diffusion which leading towards cathode copper electrolysis. This will increase the copper recovery and current productivity by increasing copper concentration.



**Figure 9.** Influence of the concentration of copper molarity on current and copper yield

#### 4. Conclusions

[Bmim][BF<sub>4</sub>] and [Emim][Cl] ionic liquids might be chosen as excellent and appropriate solvent, which increased the leaching efficiency of copper under appropriate effective circumstances as solution for the influence of leaching temperature and time. Where concentration of copper molarity is 0.23 mol/L in BmimPF<sub>6</sub>-Cu(PF<sub>6</sub>)<sub>2</sub> ionic liquid solution, as theoretical copper recovery efficiency 85% has been achieved with a current efficiency of 69%.

#### Conflict of interest

The authors declare that there is no conflict of interest regarding the publication of this article.

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