

Calcined sugar scum as a low-cost adsorbent for dye removal from aqueous solution: equilibrium, kinetic and modeling

El maguana Y.*, Elhadiri N., Benchanaa M. and Chikri R.

Research Laboratory on Materials Reactivity and Process Optimization "REMATOP", Department of Chemistry, Faculty of Science Semlalia, Cadi Ayyad University, B.P. 2390, Marrakech, Morocco

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*to whom all correspondence should be addressed: e-mail: youssefelmaguana@gmail.com

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Graphical abstract



Abstract

Sugar-refining process in sugar industry produces a high amount of waste that can be used as secondary source material. This waste was calcined and used as low-cost adsorbent for the removal of methylene blue (MB) and methyl orange (MO) as models for cationic and anionic dyes. The kinetic and equilibrium adsorption have been investigated to determine the adsorption mechanisms and the adsorption capacities. The pseudo-first order, the pseudo-second order and the intraparticle diffusion models were used to examine the adsorption kinetic. Adsorption isotherm was modeled using Langmuir and Freundlich models. MB adsorption process can be best described by the pseudo-first order and Langmuir isotherm models while MO adsorption process was best fitted to the Langmuir isotherm with a monolayer maximum adsorption capacity of 40.28 mg/g. Moreover, both pseudo-first order and pseudo-second order models were appropriate to describe the adsorption process of MO. The percentage removal of the calcined sugar scum powder (CSSP) was found greater than 98% and 87% for MB and MO, respectively. The results showed that (CSSP) is a powerful adsorbent for the removal of cationic and anionic dyes.

Keywords: Calcined sugar scum, adsorption kinetic, adsorption isotherm, dye.

1. Introduction

The increase of population growth, along with improving economic growth, has brought serious problems including

the continuous increase in the amount of industrial solid wastes. These wastes can contain hazardous components that pollute and endanger the environment and cause harmful effects on human and animal health, but they can be used as secondary raw materials. Thus, the scientific community has become increasingly interested in the waste management which can be valorized and used for various applications because they are abundant and renewable. The utilization of industrial solid wastes as raw materials has a positive impact in environment protection by reducing solid wastes and also producing of low-cost materials with high added value. Consequently, the industrial solid wastes have been used in various domains such as manufacturing of adsorbents, production of energy fuels through fermentation processes, production of thermal energy by combustion, preparation of composts, etc (Cerda et al., 2018; Du et al., 2018; El maguana et al., 2018, 2019; Gautam et al., 2014; Marcelo et al., 2017; Omo-Okoro et al., 2018). The utilization of industrial wastes as raw materials for the production of adsorbents has a positive impact in the protection of the environment by reducing industrial solid wastes and minimizing the cost of wastewater treatment (Athalathil et al., 2014; Ennaciri et al., 2014). Various industrial solid wastes have been used as precursors for the preparation of efficient and inexpensive adsorbents such as fly ash and red mud (Wang et al., 2005), wood sawdust (Foo and Hameed, 2012), olive stones and sugar cane bagasse (Moubarik and Grimi, 2015), marble dust (Haddad et al., 2015), Shrimp Shell (Singh et al., 2018), etc.

Adsorption has been found a very efficient technique for wastewater depollution in terms of its capacity to remove a broad range of pollutants, fast adsorption kinetics, simplicity of design, and low cost. Among these pollutants, the dyes used in several sectors such as textiles, cosmetics, plastics, pigments units, leather, and paper industries. They have been considered as the primary pollutant due to their stability and low biodegradability, and therefore cause the degradation of the ecosystem and harmful effects on human and animal health (Elgarahy *et al.*, 2019). So, the removal of dyes from wastewater becomes environmentally important because

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even in low concentration of dye in water can be toxic and highly visible. Therefore, the scientific community has contributed to the treatment of industrial effluents by developing effective dyes removal techniques. The effectiveness of the adsorption for the removal of a wide variety of dyes from wastewater has made it an ideal alternative to other expensive treatment techniques (Crini, 2006; Salleh *et al.*, 2011).

Among solid wastes that could be valorized, the sugar scum powder resulting from the sugar-refining process through juice carbonatation. This waste is separated from the sugary juices using filtration and contains primarily precipitated calcium carbonate as well as minerals and organic materials removed in juice purification (El maguana et al., 2020). It is disposed of in open fields or sold as compost to farmers to neutralize acidic soils and improve their structures. In our previous study (El maguana et al., 2018), we used the sugar scum powder for the preparation of an appropriate adsorbent for the methylene blue removal by optimizing the calcination temperature and time. In the present study, the adsorption properties of the calcined sugar scum powder for methylene blue and methyl orange as models for cationic and anionic dyes have been studied. Furthermore, the kinetic and equilibrium adsorption have been investigated to determine the adsorption mechanisms and the adsorption capacities.

2. Materials and methods

2.1. Materials

The calcined conditions of the sugar scum powder used in this study were described previously in our paper (El maguana *et al.*, 2018) (calcination temperature 986°C, calcination time61 min, and in air). CSSP was sieved to obtain particles size less than 200µm. MB and MO used as adsorbates in the present study and without further purification were supplied by Merck. A stock solution was prepared by dissolving the weighted quantity of each dye in distilled water, and then solutions of desired concentrations were prepared by diluting stock solution with distilled water.

The structure of methylene blue is given by:



The structure of methyl orange is given by:



2.2. Adsorption experiments

Batch adsorption experiments have been conducted to evaluate the efficiency of CSSP to remove MB and MO dyes from aqueous solution. The experiments were performed in flasks containing a defined amount of CSSP and 100 cm³ of desired concentration of dye solution. The suspensions were mixed on a shaker at 180 rpm during a given time and separated with centrifuge. After adsorption, the residual concentration of MB or MO was determined by spectrophotometric method (UV-3100PC Spectrophotometer) at 664 nm and 462 nm, respectively.

The amount of adsorption at equilibrium (q_e) was defined as the amount of adsorbate per gram of adsorbent (in mg/g) and was calculated using the following equation:

$$q_e = \frac{C_0 - C_e}{m} \times V \tag{1}$$

The percentage removal (R%) at equilibrium was calculated using the following relationship:

$$R\% = \frac{C_0 - C_e}{C_0} \times 100$$
 (2)

Where C_0 and C_e (in mg/L) are the initial and equilibrium concentrations in aqueous solution respectively, V(L) is the volume of the solution and m(g) is the mass of the adsorbent.

2.3. Characterization techniques

CSSP was characterized by using X-ray powder diffraction (XRD) and scanning electron microscopy coupled with energy dispersive X-ray spectroscopy (SEM/EDX) to identify the various phases present in this material and also to examine the morphology and the development of porosity of CSSP as well as to determine its elemental composition (El maguana *et al.*, 2020).

3. Results and discussion

3.1. Characterization of sugar scum

The XRD pattern, presented in Figure 1, shows the presence of calcium oxide (CaO), calcium hydroxide (Ca(OH)₂), and Periclase (MgO) phases in CSIW (JCPDS card No. 01-077-2010, 01-084-1265, and 01-079-0612) in CSSP (El maguana *et al.*, 2018). The intense peak appeared at $2\theta = 37.4^{\circ}$ reveals that CaO is the main phase present in CSSP (Chraibi *et al.*, 2016; Park *et al.*, 2007).



Figure 1. XRD patterns of CSSP.

The SEM micrograph of CSSP (Figure 2) illustrates that this material is formed of agglomeration of small particles with

irregular shape. Moreover, CSSP exhibits a porous texture due to the release of carbon dioxide. The results of the elemental analysis using EDX (Figure 3) indicate that the major elements present in CSSP are calcium (62.55%) and oxygen (32.87%). In addition, small amounts of other elements (C, P, Mg, Si, S and Al) are observed for CSSP.



Figure 2. SEM of CSSP.



Lsec: 30.0 0 Cnts 0.000 keV Det: Apollo X-SDD Det

Figure 3. EDX of CSSP.



Figure 4. Effect of adsorbent dose on the adsorption of MB and MO. (t_{contact}=24 h; [MB]₀ =[MO]₀ = 100 mg/L; pH~7; T=25°C).

3.2. Adsorption studies

3.2.1. Effect of adsorbent dose on the adsorption of MB and MO

Figure 4 shows the effect of the adsorbent dose, ranging from 2 to 10 g/L, on the adsorption of MB and MO. The increase of the amount of CSSP in the solution increases the removal percent of dyes until almost 96%. This observation can be explained by the increase in the surface area of the adsorbent and hence the number of available adsorption sites for MB and MO adsorption (El Maguana *et al.*, 2019). The optimal amount of CSSP which corresponds to the maximum of MB and MO removal was found to be 4 g/L. Therefore, adsorbent dose of 4 g/L was chosen for dyes removal for further studies.

3.2.2. Effect of contact time on the adsorption of MB and MO

The evolution of the percentage removal and the adsorption capacity of CSSP for MB and MO versus contact time are shown in Figures 5 and 6. The adsorption rate was rapid at the beginning of the process due to the availability of active sites on the exterior surface and after the saturation of those active sites, the dye molecules entered to the pores of the adsorbent with a slower rate to reach the equilibrium time (El Maguana et al., 2019). The equilibrium state was established almost after 10 h for MB (Figure 5a) and after 1h for MO (Figure 5b). Thus, in the subsequent experiments, 10 h and 1 h were taken to ensure the adsorption equilibrium of MB and MO, respectively. In addition, the amounts of MB and MO adsorbed at equilibrium onto CSSP were 24.5 and 21.38 mg/g, respectively, which correspond to the percentage removal of 98% and 87% for MB and MO. It can be thus noticed that the adsorption process of MO was higher than that of MB. This can be explained by the size and structure of MB and MO molecules. The size of a molecule determines to a certain extent the liquid film diffusion and particle diffusion within the pore network of the adsorbent. When the pore size of the adsorbent corresponds with the size of the adsorbate molecule, the adsorption process will be easier and faster; provided all other factors remain constant. MO has one ring (benzene) on both sides of the azo group (-N=N-) giving a total of two rings. Its structure is symmetrical, linear, and more flexible compared to MB which is formed by three rings (two benzene rings and one heterocyclic) restricting the flexibility of the molecule. MB molecule is more bulky than MO. This above observation and discussion may be the main reason for the difference in the adsorption rates of each dye onto CSSP.

3.2.3. Adsorption kinetic modeling

The modeling of the adsorption processes is usually carried out using well-established adsorption kinetic models, which provide invaluable information on the controlling mechanisms of the adsorption process (El maguana *et al.*, 2020). The overall adsorption process may be controlled either by external or film diffusion, pore diffusion and adsorption on the pore surface, or a combination of more than one step (El maguana *et al.*, 2020). In order to predict the mechanism of the adsorption process of MB and MO onto CSSP, the experimental data were fitted by the pseudo-first order (Lagergren, 1898), pseudo-second order (Ho and McKay, 1999), and intraparticle diffusion (Weber and Morris, 1963) models.

The pseudo-first order model is given by the following equation:

$$q_t = q_e(1 - e^{-k_1 t})$$
 (3)

The pseudo-second order model is given as follows:

$$q_t = \frac{k_2 q_e^2 t}{1 + k_2 q_e t} \tag{4}$$

Where q_e (mg/g) is the adsorption amount at equilibrium, q_t (mg/g) is the adsorption amount at time t (min), and k_1 (1/min) and k_2 (g/mg/min) are the adsorption rate constants of pseudo-first order and pseudo-second order models, respectively. Kinetic parameters q_e , k_1 , and k_2 can be calculated from the plots of q_e versus t.



Figure 5. Effect of contact time on (a) MB removal and (b) MO removal. (Adsorbent dose = 4 g/L; $[MB]_0 = [MO]_0 = 100 \text{ mg/L}$; pH~7; T=25°C).

The plots for pseudo-first order and pseudo-second order kinetic models for MB and MO adsorption are presented in Figure 6a and b. The calculated parameters of these two kinetics models are presented in Tables 1 and 2.

Based on the correlation coefficient (R^2) and the adsorption capacity values, it can be deduced the model which describes the adsorption process of MB and MO onto CSSP. The results showed that the experimental data of the MB adsorption were efficiently fitted by the pseudo-first order model; higher R^2 value and the adsorption capacity calculated by this model ($q_{e,cal}$) is closer to the experimental value ($q_{e,exp}$); while both pseudo-first order and pseudo-second order models could be used to describe the adsorption process of MO onto CSSP because R^2 obtained by these two models is greater than 0.99. These results suggest that the boundary layer resistance was the rate-limiting step in the case of MB adsorption process and it was not he rate-limiting step in the case of MO adsorption process (Barka *et al.*, 2013).



Figure 6. Non-linear fits of pseudo-first order and pseudo-second order models for (a) MB adsorption and (b) MO adsorption ([MB]₀ =[MO]₀ = 100 mg/L; Adsorbent dose= 4 g/L; pH~7; T= 25°C).

The pseudo-first order and pseudo-second order kinetic models could not determine the diffusion mechanism. Hence, the intraparticle diffusion model proposed by Weber–Morris was employed to further evaluate the adsorption of the solute on CSSPand thus to predict the rate limiting steps.

The intraparticle diffusion model is expressed as follows:

$$q_t = k_{id} t^{1/2} + c \tag{5}$$

Where $q_t (mg/g)$ is the adsorption amount at time t (min), $k_{id} (mg/g/min^{1/2})$ is the adsorption rate constant of intraparticle diffusion model, and c is a constant related to the thickness of the boundary layer.

Figure 7 shows the plots of the intraparticle diffusion model of MB and MO adsorption. It can be seen that the plots did not pass through the origin, thus the intraparticle diffusion was not the only rate-controlling step of the adsorption process of both dyes, but also other mechanisms may control the rate of adsorption such as the boundary layer diffusion (Foo and Hameed, 2012). The presence of four distinct regions is clearly observed for the transfer of MB to the particles of CSSP (Figure 7a), indicating that the MB adsorption was influenced by more than one process. The first portion of the plot is attributed to the boundary layer diffusion of MB molecules. Thereafter, the second and third parts were ascribed to the intraparticle diffusion which was the gradual adsorption. In fact, the slope of the linear portion indicates the rate of the adsorption process; the lower slope corresponds to a slower adsorption process

(Oguntimein, 2015). Thus, the rate of the diffusion of MB molecules through boundary layer film in the initial stage of the adsorption process was slowerthan the rate of the intraparticle diffusion because the slope of the first linear portion was lowerthan of the second and third linear portions. Finally, the last portion is attributed to the final equilibrium stage for which the intraparticle diffusion slows down due to the low concentration dye in the aqueous solution. For MO adsorption, the plot was **Table 1.** Kinetic parameters for MB adsorption onto CSSP

separated into three steps (Figure 7b). The first step was a rapid diffusion through liquid film to the adorbent exterior surface. The second and third steps were ascribed to the intraparticle diffusion and the final equilibrium stage, respectively. Initially, MO molecules are quickly adsorbed onto the surface of CSIW, and when saturation is reached, MO molecules are diffused into the interior of adsorbent particles.

Model		Parameters		
Pseudo-first order —	q _{e,cal} (mg/g)	k ₁ (1/min)	R ²	q _{e,exp} (mg/g)
	24.10± 0.26	61.6 10 ⁻⁴ ±2.88 10 ⁻⁴	0.996	24.50±0.22
Pseudo-second order —	q _{e,cal} (mg/g)	k ₂ (g/mg/min)	R ²	
	27.71±0.43	2.68 10 ⁻⁴ ±0.21 10 ⁻⁴	0.995	
Table 2. Kinetic parameters for MO adsorption onto CSSP				
Model	Parameters			
Pseudo-first order —	q _{e,cal} (mg/g)	k ₁ (1/min)	R ²	q _{e,exp} (mg/g)
	21.45± 0.15	26.44 10 ⁻² ±2.30 10 ⁻²	0.998	21.38±1.01
Pseudo-second order —	q _{e,cal} (mg/g)	k ₂ (g/mg/min)	R ²	
	21.81±0.08	5.27 10 ⁻² ±0.52 10 ⁻²	0.999	





Figure 7. Plot of intraparticle diffusion model for (a) MB adsorption and (b) MO adsorption ([MB]₀ =[MO]₀ = 100 mg/L; Adsorbent dose= 4 g/L; Ph~7; T= 25 °C).

3.2.4. Adsorption isotherm modeling

The adsorption isotherm describes the interaction between the adsorbate molecules and the adsorbent when the system reaches the equilibrium (El maguana *et al.*, 2020). It provides the qualitative information on the nature of adsorbate-adsorbent surface interactions and

could be used to evaluate the adsorption capacity (El maguana *et al.*, 2020). The experimental data of MB and MO adsorption isotherms obtained at 20 °C were fitted to the Langmuir and Freundlich models to find which one can be used to describe the adsorption process of these two dyes onto CSSP. Langmuir equation assumes the monolayer adsorption on a homogenous surface without interaction between adsorbates while the Freundlich isotherm was based on the assumption of the multilayer adsorption on heterogeneous surface (El maguana *et al.*, 2020; El Maguana *et al.*, 2019).

The Langmuir isotherm equation is expressed as:

$$q_e = \frac{q_m K_L C_e}{1 + K_L C_e}$$
(6)

The Freundlich isotherm equation is given as:

$$q_e = K_F C_e^{1/n}$$
(7)

Where C_e (mg/L) is the equilibrium concentration of adsorbate, q_e (mg/g) the amount of adsorption at the equilibrium, q_m (mg/g) is the monolayer adsorption capacity, n is the Freundlich intensity constant, and K_L and K_F are the Langmuir and Freundlich constants, respectively.

The adsorption isotherm of MB onto CSSP, at temperature 20 °C, is shown in Figure 8a. According to the classification of Giles (Giles *et al.*, 1960), this adsorption isotherm displayed a C-type curve, indicating that the adsorbate molecules penetrate into the solid more readily than those of the solvent Moreover, this curve is characterized by the constant partition of solute between the solution and the adsorbent surface, right up the maximum possible adsorption, where an abrupt change to a horizontal plateau occurs. Figure 8b presents the adsorption isotherm of MO onto CSSP, at temperature

20 °C. According to the classification of Giles (Giles *et al.*, 1960), it is a L-type curve, suggesting a relatively high affinity between the solid surface and the solute. As more sites in the adsorbent are filled, it becomes increasingly difficult for solute molecules to find a vacant site available.



Figure 8. Adsorption isotherm of (a) MB adsorption and (b) MO adsorption (Adsorbent dose = 4 g/L; pH 7 ; T= 25 °C; t_{contact} =10 h for MB and 1 h for MO).

 Table 3. Langmuir and Freundlich isotherm parameters for MB adsorption onto CSSP

Model	Parameters			
Lanamuin	q _m (mg/g)	K _L (L/mg)	R ²	
Langmun	57.34± 3.46	0.016±0.007	0.96	
European all'als	n	K _F ((mg/g)(L/mg) ^{1/n})	R ²	
Freundlich	1.17±0.05	1.04±0.18	0.98	

 Table 4. Langmuir and Freundlich isotherm parameters for MO adsorption onto CSSP

Model	Parameters			
Longenerin	q _m (mg/g)	K∟ (L/mg)	R ²	
Langmuir	40.28± 2.32	7.80·10 ⁻² ±1.00·10 ⁻²	0.99	
Fraundlich	n	KF ((mg/g)(L/mg) ^{1/n})	R ²	
Freunalich	2.04 ±0.27	5.3581±1.06	0.87	

Calculated parameters of Langmuir and Freundlich isotherms along with R^2 values are listed in Table 3 and Table 4. The values of correlation coefficients showed that the isotherm equilibrium data of MB adsorption were well fitted to the Freundlich isotherm (R^2 =0.98) while the isotherm equilibrium data of MO adsorption were best fitted to the Langmuir isotherm with high regression coefficient (R^2 =0.99). These results show that the

mechanisms involved in adsorption of MB and MO onto CSSP are different, depending on the nature of dye molecules. The adsorption process of MB occurred over a multilayer adsorption on the surface of CSSP with a different energy distribution. Furthermore, the value of 1/n was found between 0 and 1, which indicates a favorable adsorption of MB onto CSSP. The results also demonstrated that the adsorption process of MO occurred over a monolayer adsorption on the surface of CSSP without interaction between adsorbates. The maximum monolayer capacity for the MO adsorption onto CSSPwas found to be 40.28 mg/g at 20 °C.

4. Conclusion

Kinetic and equilibrium studies were conducted for the adsorption of cationic and anionic dyes from aqueous solutions onto CSSP to study the adsorption properties. The results showed that the sugar scum powder is a suitable precursor for the production of adequate adsorbent for dyes removal from industrial effluents. The adsorption isotherms of MB and MO fitted well to the Freundlich and Langmuir models, respectively. The adsorption processes of MB can be described by the pseudo-first order kinetic model. Both pseudo-first order and pseudo-second order models could be used to describe the adsorption process of MO. The percentage removal of CSSP, at pH~7 for an adsorbent dose of 4 g/L and an initial dye concentration of 100 mg/L at 25 °C, was found greater than 98% and 87% for MB and MO, respectively. The above results show that the obtained adsorbent is effective for removing dyes from aqueous solution.

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