

1 **Purification of waste water from cationic dye using SPGMA polymer:**
2 **Isotherm and Kinetic study**

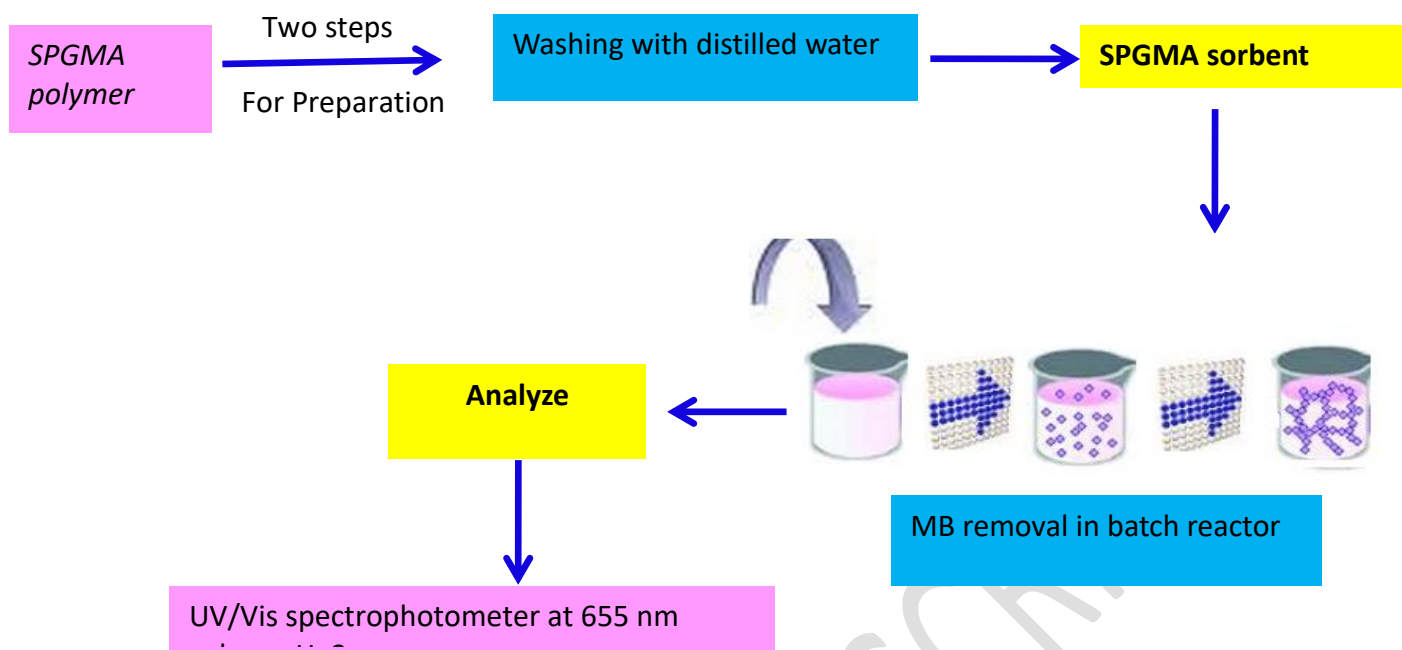
3 **M. A. Abu-Saied¹, Nahla. A. Taha^{2*}**

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5
6 ¹ Polymer Materials Research Department, Advanced Technology and New Materials
7 Research Institute, City for Scientific Research and Technology Applications (SRTACITY),
8 New Borg El-Arab City 21934, Alexandria, Egypt

9
10 ² Fabrication Technology Department, Advanced Technology and New Materials
11 Research Institute, City for Scientific Research and Technology Applications (SRTACITY),
12 New Borg El-Arab City 21934, Alexandria, Egypt

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14 *Corresponding author: Nahla Ahmed Taha,
15 E.mail: nahlataha_1982@yahoo.com , Tel: 00201005289679
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ACCEPTED MANUSCRIPT



Graphical abstract

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47 ABSTRACT

48 One of the known methods for dye removing from waste water is using sorbent material for fine
 49 removal of dye .The nano- cation exchanger Sulphonated poly glycidyl methacrylate (SPGMA
 50 polymer) was used as sorbent material for removing one of the common cationic dyes. SPGMA
 51 polymer was prepared and characterized to ensure its surface ability to sorb dye. Percentage
 52 removal of Methylene Blue using SPGMA polymer was studied by changing different parameters
 53 as sorbent amount, stirring speed, pH and solution temperature. The maximum value for dye
 54 removal was about 98%. Adsorption data from experimental work shows that the results fit the
 55 pseudo first order model for all parameters studied except for pH study fits pseudo second order.
 56 Also sorption mechanism for SPGMA polymer was studied for different dye concentration.

57 **Key words:** Methylene Blue, SPGMA, Isotherm, Kinetic, Adsorption.

58

59 **1. Introduction**

60 One of cationic dyes is Methylene blue (MB) which used in various industries such as cotton, pulp,
61 wool, paper, leather etc., to color their final products. The outlet of these industries containing huge
62 amount of different dyes, discharged this types of dyes into waters drain, cause dangerous to the
63 environment (Gad and El-Sayed, 2009). Acute exposure to MB dye will cause increased heart rate,
64 shock, Heinz body formation, vomiting, cyanosis, jaundicem and quadriplegia (Hameed and
65 Ahmad,2009).

66 Various methods such as chemical, physical, and biological processes have been used trying to
67 remove of cationic dyes from aquatic media (Barka et al., 2010, Bielska and zymanowski ,2006,
68 MohyEldin et al., 2016, Elahmadi et al., 2009, Karim et al., 2009, Khadhraoui et al., 2009, Lodha
69 and Chaudhari ,2007). However, all of the methods have some limitation and none of the processes
70 described above were successful in removing color from wastewater completely. Dye removal
71 process is the process calling Adsorption. Currently, most effective adsorbent is activated carbon.
72 Which is high cost in production and regeneration this reasons make it uneconomical (Wang et al.,
73 2005). Nowadays, there is an interest in using cheap and potential materials for the adsorption of
74 reactive dyes. Several adsorbents were reported in the literatures such as clay (Tehrani-Bagha et al.,
75 2011) , zeolite (Han et al., 2009) , fly ash (Rastogi et al., 2008), silica gel (Kushwaha et al., 2010)
76 and chitosan (Mahmoodi et al.,2011) for the adsorption of basic dyes from aqueous solution.

77 In this work decolorize of Methylene blue dyes were studied using prepared polymer (SPGMA). To
78 study the capability of color removal, different parameters that affect the adsorption process (such
79 as time, pH, and dosage of adsorbents, temperature and stirring speed) was studied. The kinetic
80 models and equilibrium studies also carried out to substantiate the relationship with the
81 experimental data for the adsorbent.

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85 2. Materials and methods

86 2.1. Preparation of methylene blue stock solution

87 The cationic dye (MB dye) was from "NICE chemicals pvt.ltd company". The stock solution was
88 prepared by dissolving 1.00 g of MB dye in 1000 mL distilled water. Diluting the prepared stock
89 solution with distilled water to make Different concentrations for experiments.

90 2.2. Preparation of Adsorbent material (SPGMA polymer)

91 Sulphonated poly (glycidyl methacrylate) nano-cation exchanger (SPGMA) were prepared by two
92 steps. First, general procedure for photo ATRP of GMA was as follows. To a 10 mL Schlenk tube
93 containing CuBr₂ and TPMA, evacuated and filled with argon. Argon-purged anisole was added
94 under argon atmosphere. Sonicate the mixture in the Schlenk tube for 5 min to form a
95 CuBr₂/TPMA complex. Subsequently GMA purged with argon and BPN was added to the Schlenk
96 tube under argon atmosphere. The mixture was degassed by three freeze-pump-thaw cycles and
97 backfilled with argon. Photo polymerization with light of $\lambda > 350$ nm was performed using a
98 medium-pressure mercury lamp in a Spectromat apparatus (Ivoclar AG, Lichtenstein, glass filter λ
99 = 350-550 nm). To prevent heating of the sample during irradiation, the Schlenk tube was placed
100 into a double-layer glass tube. In the outer layer of the finger, water thermo stated to 25°C was
101 circulated. Second, the epoxy groups of PGMA chains were reacted with sodium sulphite (Elkady et
102 al., 2011, Abu-Saied et al., 2013, MohyEldin et al ,2010, MohyEldin et al., 2011, Abu-Saied et al.,
103 2017) , dissolved in alcoholic aqueous solution at 80°C for 2 h. Discharge the excess of sodium
104 sulphite solution after centrifugation at 14,000 rpm for 30 min using ultra speed centrifuge ,
105 distilled water used in washing to remove any un-reacted sodium sulphite .The details of the
106 preparation and characterization of SPGMA polymer published before (Abu-Saied et al., 2015)

107 2.3. Experimental methods and measurements

108 Batch adsorption technique was used in this work Put 100 mL of different dye concentration on
109 rotary shaker , add different weighted adsorbent to the experimental flasks . Let solution to shake,
110 different samples at different time intervals were taken out from the flasks and separated by

111 decantation ,then remaining MB dye concentration was analyzed using UV/Vis spectrophotometer
112 at 655 nm (Ultrospec 2000 - Pharmacia Biotech). The effect of various important parameters in
113 adsorption process as adsorbent dose, stirring speed, pH values and temperature was studied.

114 The equation used in calculating the amount of MB dye adsorbed by SPGMA polymer was:

$$115 \quad q = (C_0 - C_e) * V / W \quad (1)$$

116 Where q (mg/g) is the MB dye adsorbed by SPGMA polymer , C₀ and C_e (mg/l) are the initial and
117 equilibrium concentrations of the MB dye, respectively, V (l), the initial volume of MB dye
118 solution, and W (g), the weight of the polymer.

119 The percentage removal of MB dye from solution was by using the following equation:

$$120 \quad \%Re = (C_0 - C_e) / C_0 * 100 \quad (2)$$

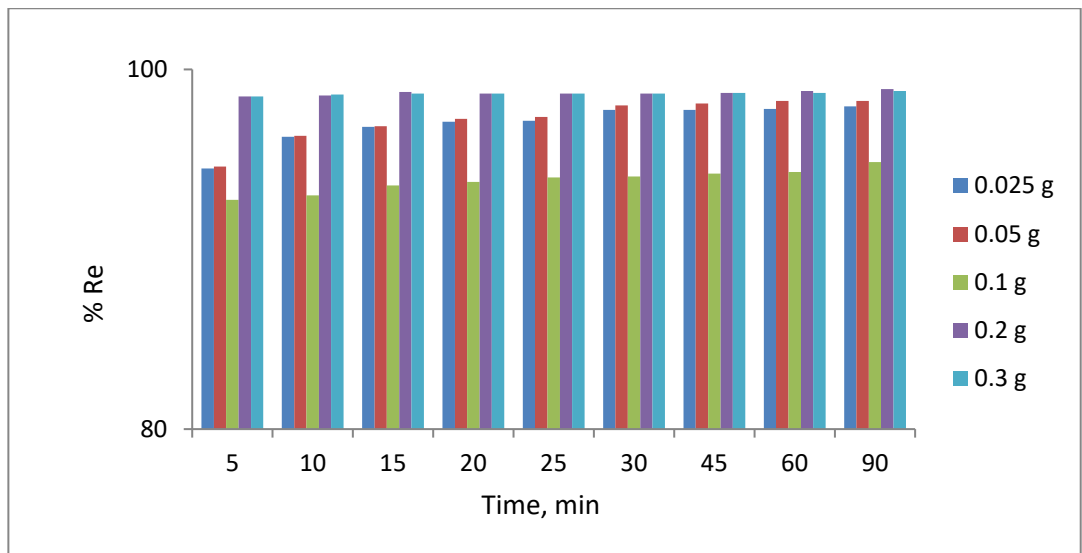
121 Where C₀ and C_e (mg/l) are the initial and equilibrium concentrations of the MB dye.

122 **3. Results and discussion:**

123 *3.1. Effect of sorbent dose adsorption*

124 Fig (1) illustrates the adsorption removal from 20 ppm dye concentration. The percentage removal
125 of dye was slightly increased with increasing SPGMA polymer dose from 0.025 g to 0.3 g along the
126 total period of the experiment (90 min) to reach 98% for 0.2 and 0.3 g of sorbent material .This
127 result concludes that more surface area was made due to increase of adsorbent mass .Therefore,
128 the total number of active sites increases which increase the percentage removal of dye (Al-Qodah,
129 2000)

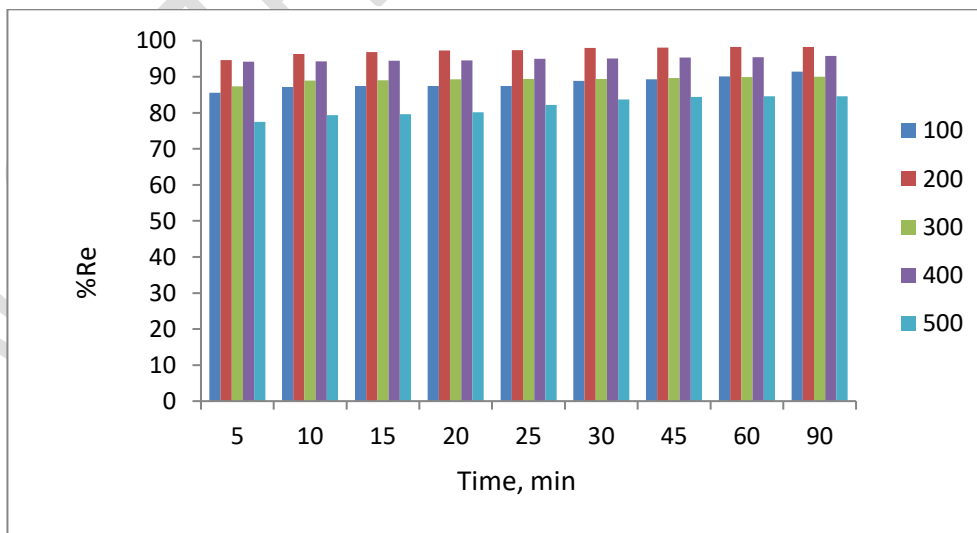
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131
 132 **Figure 1.** Effect of sorbent dose on adsorption of MB by SPGMA polymer
 133 (dye concentration: 20 mg/l; stirring speed 200 rpm; contact time: 90 min).
 134

135 *3.2. Effect of changing the stirring speed*

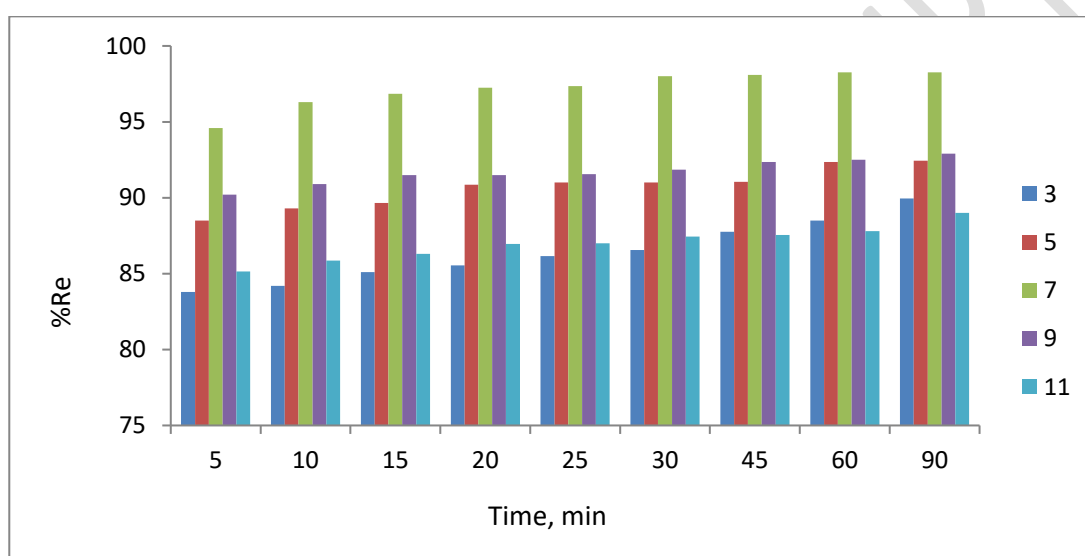
136 Fig (2) shows the adsorption removal by changing the stirring speed from (100-500 rpm) at
 137 different time intervals from 5 to 90 min . The figure concludes that the stroke speed affect slightly
 138 as the percentage removal decreased by increasing stirring speed, and the highest percentage removal
 139 of dye was at 200 rpm.



140
 141 **Figure 2.** Effect of stirring speed on adsorption of MB by SPGMA polymer
 142 (dye concentration: 20 mg/l; sorbent dose: 0.05g ; contact time: 90 min).
 143

144 3.3. Effect of pH change

145 Fig (3) shows adsorption capacity of MB dye by increasing pH value from 3 to 11. The percentage
146 removal of dye increase with increasing pH value to reach maximum value at pH= 7 which record
147 about 98 % dye removal, then decrease to reach the lowest value at pH= 11, so for future studies,
148 the optimum pH adopted at pH 7. Also the increasing time from 5 to 90 min for all pH values do
149 not affect the removal percentage.

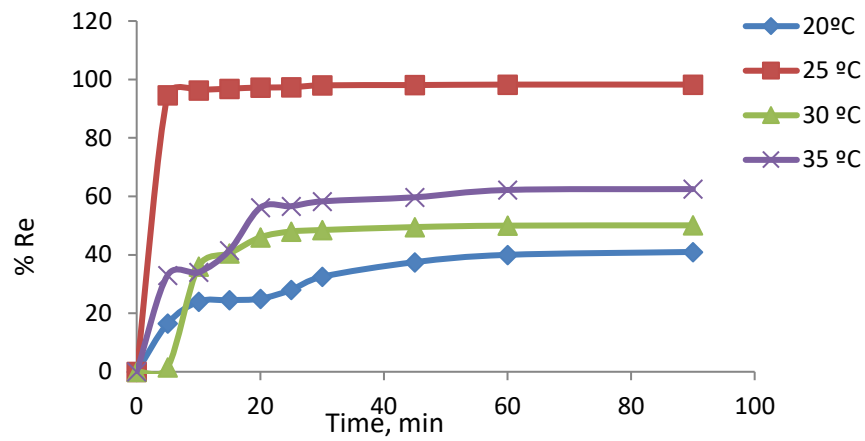


150

151 **Figure 3 .** Effect of pH on adsorption of MB by SPGMA polymer
152 (dye concentration: 20 mg/; stirring speed:200 ; sorbent dose: 0.05g ; contact time: 90 min).
153

154 3.4. Effect of temperature variation

155 As illustrated in Fig (4) , the decolonization of MB dye was tested for wide range of temperature
156 from 20 to 35 °C. The results cleared that by increasing the temperature of solution the percentage
157 dye removal increased. To reach the maximum value at 25°C. While by increasing time for each
158 temperature, it does not have great effect. The temperature effect on adsorbtion process concludes
159 in two major effects. Increasing the temperature is known to increase the rate of diffusion of the
160 adsorbate molecules across the external boundary layer and in the internal pores of the adsorbent
161 particles due to the decrease in the solution viscosity (Lagergren,1898)



162

163 **Figure 4** . Effect of Temperature on adsorption of MB by SPGMA polymer
 164 (dye concentration: 20 mg/l; sorbent dose: 0.05g ;; stirring speed: 200; pH:7; contact time: 90 min).
 165

166 **4. Adsorption kinetics study:**

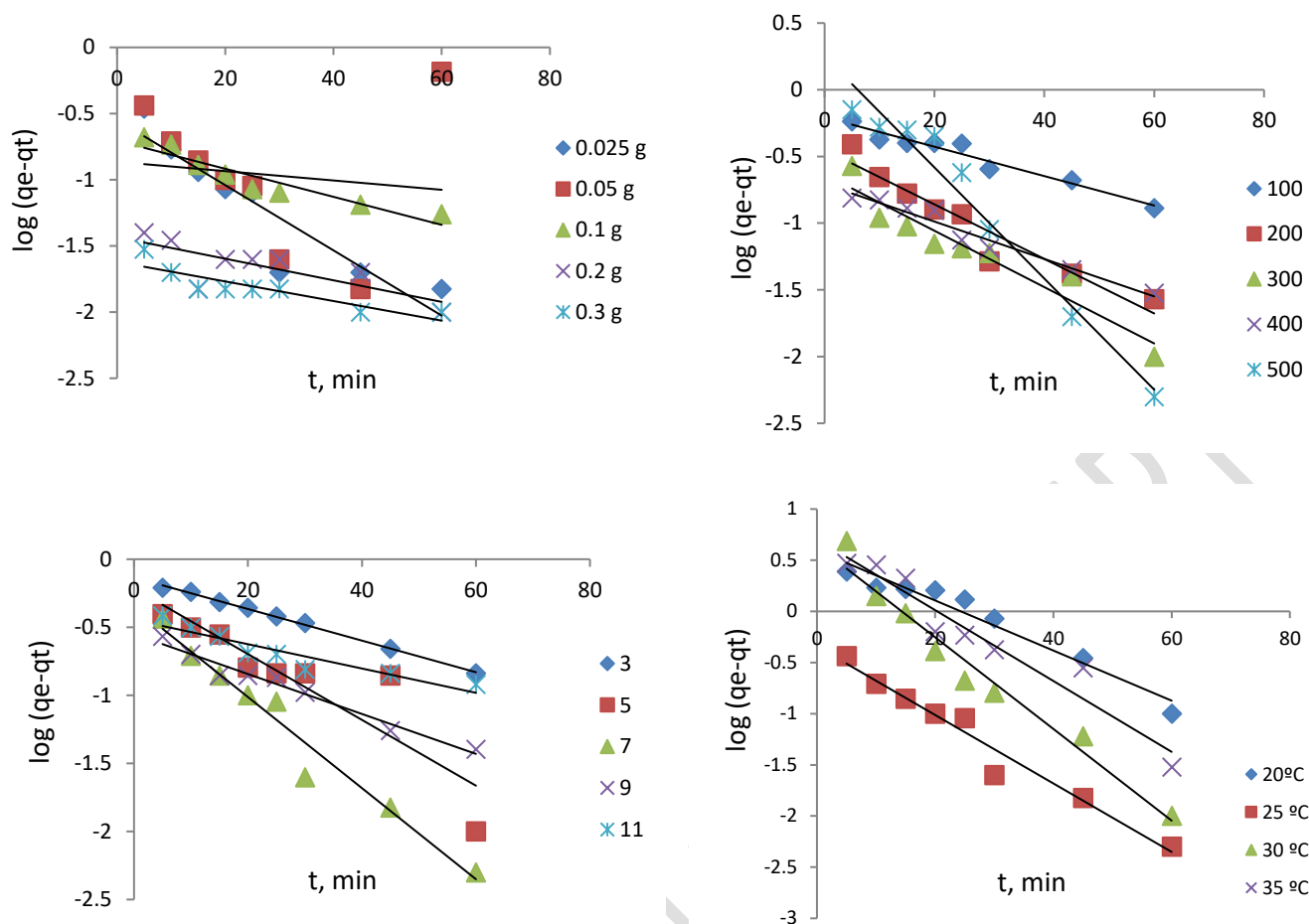
167 The pseudo-first-order kinetic equation of Lagergren method for adsorption analysis (Ho and
 168 McKay, 1998) :

169
$$\frac{dq_t}{dt} = k_1 (q_e - q_t) \quad (3)$$

170 By integrating equation (3) for boundary conditions as $t=0$ to $t = t$ and $q_t=0$ to $q_t= q_t$,

171
$$\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303} t \quad (4)$$

172 Where the equilibrium rate constant is k_1 (1/min), q_e is the MB dye adsorbed on the surface at
 173 equilibrium (mg/g), q_t is the MB dye adsorbed at different times (mg/g). The adsorption rate
 174 constant (k_1) for MB sorption by SPGMA polymer powder was determined from the figure which
 175 illustrates $\log (q_e - q_t)$ against time t (as in Fig. 5). The pseudo-first-order model at different
 176 parameters studied are summarized in Table (1)



177

178 **Figure 5.** Pseudo-first-order kinetics for adsorption of MB onto SPGMA polymer at different
 179 parameters.

180 While equation (5) expressed pseudo-second-order kinetics (Ho and McKay,2000, Weber and
 181 Morris,1963):

$$182 \quad \frac{dq_t}{dt} = k_2 (q_e - q_t)^2 \quad (5)$$

183 As k_2 is the dye adsorption rate constant, q_e is the amount of MB dye adsorbed at equilibrium
 184 (mg/g) and q_t is the amount of MB dye adsorbed at different time intervals t (mg/g). Separating the
 185 variables in Eq. (7) gives:

$$186 \quad \frac{dq_t}{(q_e - q_t)^2} = k_2 dt \quad (6)$$

187 By Integrating equation (6) for the boundary conditions $t=0$ to $t = t$ and $q_t=0$ to $q_t = q_t$:

188
$$\frac{1}{q_e - qt} = \frac{1}{q_e} + k_2 t \quad (7)$$

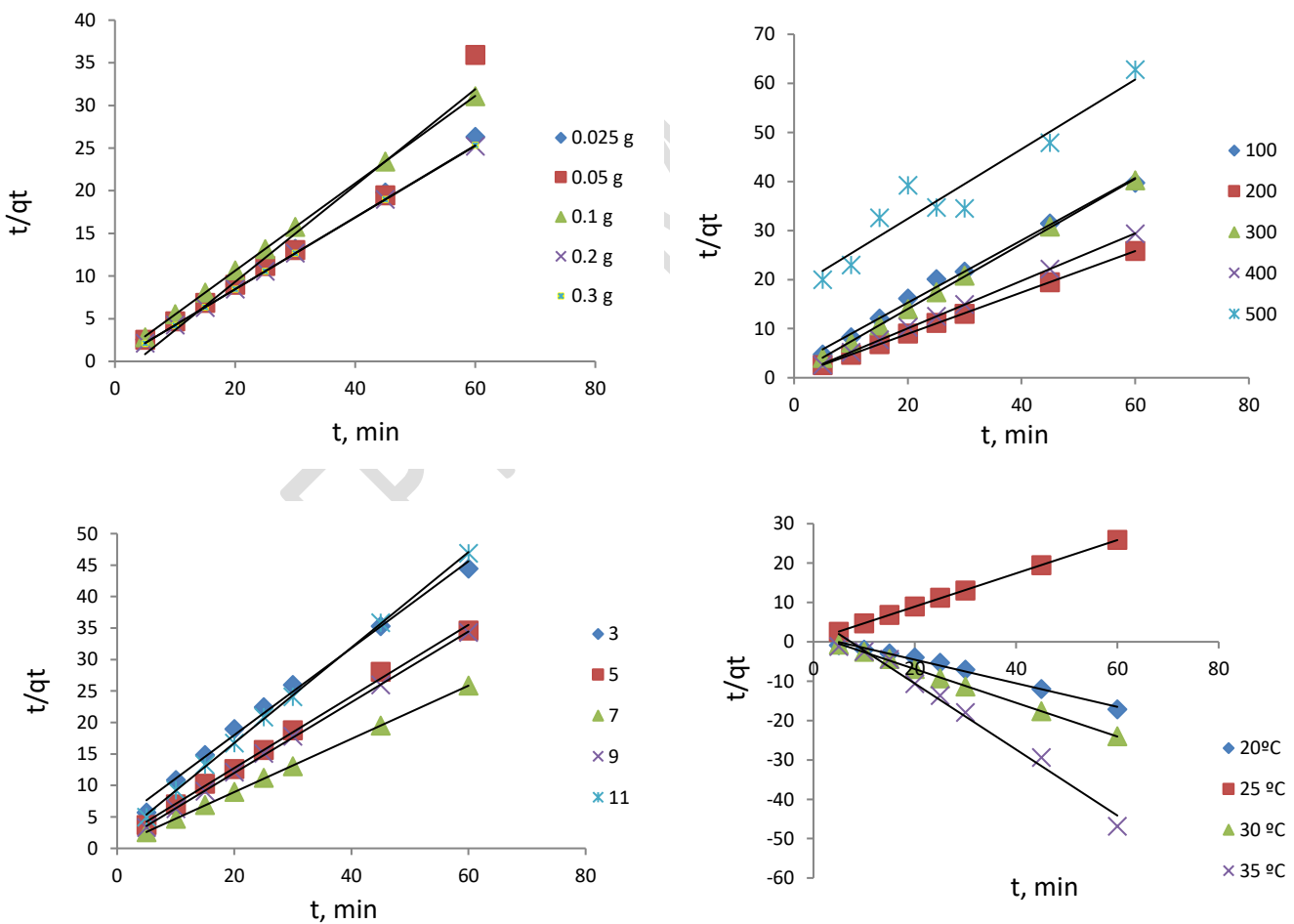
189 by rearranging Eq. (7) the equation give the following one :

190
$$qt = \frac{t}{\left(\frac{1}{k_2 q_e^2}\right) + \left(\frac{t}{q_e}\right)} \quad (8)$$

191 Which has a linear form of equation (9) :

192
$$\frac{t}{qt} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t \quad (9)$$

193 As the equilibrium adsorption capacity (q_e), and second order constants k_2 (g/mg min) can be
 194 determined experimentally from the slope and intercept of t/q_t versus t figure as in (Fig.6).



195
 196 **Figure6.** Pseudo-second-order kinetics for adsorption of MB onto SPGMA polymer at different
 197 parameters

198 Table (1) present he coefficients of the pseudo-first- and second-order adsorption kinetic models.
 199 According to values of R^2 for the pseudo-first-order model and the q values ($q_{e,cal}$) calculated for
 200 sorbent dose, stirring speed and temperature it seems fitted to it . While, the pseudo-second-order
 201 model better represented the adsorption kinetics and this suggests for pH study. The overall rate of
 202 MB dye adsorption process appeared to be controlled by chemical process.

203 **Table (1)** Comparison of the pseudo-first-order, pseudo-second-order adsorption rate constants and
 204 calculated and experimental q_e values obtained at different initial MB concentrations for different parameters
 205 studied

| Dye system | $q_{e,exp}$ mg/g | Pseudo first order model | | | Pseudo second order model | | |
|---|--------------------------------------|--|---|--|---|---|--|
| | | K_1 min ⁻¹ | q_{e1} mg/g | R^2 | K_2 g/mg.min | q_{e2} mg/g | R^2 |
| 1 Sorbent dosage n= 200 rpm C ₀ =20 mg/l w= 0.025g w= 0.05g w= 0.1g w= 0.2g w= 0.3g | 0.41 0.35 1.03 0.22 0.24 | 0.0567 0.0081 0.0244 0.0189 0.0170 | 0.283 0.1366 0.8968 0.0368 0.0239 | 0.847 0.814 0.879 0.603 0.781 | 13.35 -1.57 10.36 122.39 234 | 5.378 3.133 3.807 5.666 5.626 | 1 0.949 1 1 1 |
| 2- rpm W= 0.05g pH=7 C ₀ =20 mg/l rpm= 100 rpm= 200 rpm= 300 rpm= 400 rpm=500 | 1.72 0.35 2 0.85 3.08 | 0.0253 0.0469 0.0486 0.0322 0.0958 | 1.222 0.3549 1.832 0.696 2.779 | 0.949 0.922 0.911 0.962 0.965 | 0.155 0.354 0.579 0.612 0.029 | 1.5745 2.3702 1.5087 2.066 1.4098 | 0.9939 0.9999 0.9998 0.9998 0.9196 |
| 3- pH W= 0.05g rpm=200 C ₀ =20 mg/l pH=3 pH=5 pH=7 pH=9 pH=11 | 2.01 1.51 0.35 1.42 2.2 | 0.0267 0.0557 0.0772 0.0338 0.0205 | 0.735 0.611 0.453 0.282 0.358 | 0.9973 0.8035 0.9665 0.9698 0.8839 | 0.1138 0.2314 0.366 0.424 0.365 | 1.449 1.759 0.366 1.779 1.3989 | 0.9927 0.9968 0.999 0.9996 0.9996 |
| 4-Temperature W=0.05g rpm=200 C ₀ =20 mg/l T=20 T=25 T=30 T=35 | 4.8 0.35 9.98 7.5 | 0.0564 0.0772 0.1032 0.0797 | 3.628 0.453 8.392 5.062 | 0.9524 0.9665 0.9665 0.936 | 0.062 0.366 0.11 0.113 | 3.339 2.365 2.332 1.192 | 0.9896 0.999 0.9994 0.9834 |

206

207 **5. Mechanism of Sorption Process:**

208 In a solid–liquid adsorption process: the transfer of adsorbate is controlled either by boundary layer
209 diffusion (called external mass transfer) or by intraparticle diffusion (called mass transfer through
210 the pores), or by both processes. Generally accepted the adsorption dynamics consists of three
211 consecutive steps: The first is the transport of adsorbate molecules from the bulk solution to the
212 external surface of the adsorbent by diffusion through the liquid boundary layer, second is the
213 diffusion from the external surface and into the pores of the adsorbent, finally, Adsorption on the
214 active sites on the internal surface of the adsorbent pores.

215 The overall rate of adsorption is controlled by film or intraparticle diffusion, or by combination of
216 both. The rate controlling step in systems characterized by dilute concentrations of adsorbate, poor
217 mixing, and small particle size adsorbent is the boundary layer diffusion. Also, it has been cleared
218 in many studies that boundary layer diffusion is dominant during the initial adsorbate uptake, then
219 gradually adsorption rate becomes controlled by intraparticle diffusion after the adsorbent's external
220 surface is loaded with the adsorbate.

221 Equation (10) present intraparticle diffusion parameter, $k_i(\text{mg/g min}^{0.5})$ (Ho and McKay, 1998):

$$222 \quad q = k_i t^{0.5} + c \quad (10)$$

223 as q is the MB dye adsorbed (mg/g) at time t , while k_i is intraparticle diffusion constant (mg/g min),
224 and c is the intercept. It can be calculated from the slope of the linear plot of q_t versus $t^{1/2}$. The slope
225 of the curve of different initial concentrations shows the k_{id} values as shown in Table (2).
226 Theoretically, the graph of k_i versus $t^{0.5}$ should separate at least to four linear regions that represent
227 boundary layer diffusion, followed by intraparticle diffusion in macro, meso, and micro pores.
228 These four regions are followed by a horizontal line representing the system at equilibrium. Also,
229 the figure of dye uptake, illustrate q_t versus square root of time ($t^{1/2}$) should be linear if intraparticle
230 diffusion is involved in dye adsorption process and if these lines pass through the origin point,
231 intraparticle diffusion is the rate controlling step. If the lines do not pass through the origin point ,
232 this is indicate of some degree of boundary layer control and this further show that the intraparticle

233 diffusion is not the only rate-limiting step. The boundary layer thickness can be indicated by the
234 intercept value as the intercept increase, the greater the boundary layer effect.

235 **Table (2)**. Intraparticle diffusion constants for different initial MB concentrations

| Initial concentration (mg/L) | k_{id} (mg/g min ^{1/2}) | C | R^2 |
|------------------------------|-------------------------------------|--------|--------|
| 5 | 0.0483 | 1.8282 | 0.9303 |
| 10 | 0.0195 | 1.8679 | 0.8432 |
| 15 | 0.0291 | 1.8025 | 0.8335 |
| 20 | 0.0272 | 1.7375 | 0.9127 |
| 25 | 0.1687 | 0.3519 | 0.8149 |

236

237

238 **Conclusions:**

239 The present results in this study show that the SPGMA polymer has high ability to adsorb
240 methylene blue dye from wastewater with removal percentage about 98% and more. Different
241 parameters are studied and Adsorption kinetics was studied .comparing q calculated and q
242 experimental shows that the results follows pseudo first order for sorbent dose, rpm and temperature
243 while fitted pseudo second order for pH. Also the results clear that the overall MB dye adsorption
244 rate controlled by chemical process. This research concludes the ability of SPGMA polymer in
245 removal of cationic dye with high removal efficiency.

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