

Optimization of degradation of ciprofloxacin antibiotic and assessment of degradation products using full factorial experimental design by Fenton Homogenous process

Rakshandehroo G.R., Salari M.* and Nikoo M.R.

Department of Civil and Environmental Engineering, Shiraz University, Shiraz, Iran

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*to whom all correspondence should be addressed: e-mail: m.salari@shirazu.ac.ir

Abstract

The Pharmaceutical contaminants specialist antibiotics into environment can create problems for both human health and environment. Ciprofloxacin (CIP), an antibiotic Fluoroquinolones group, has recently been used widely for infections treatment. The main purpose of the research was to develop a Full factorial method for degradation of CIP in aqueous solution by Fenton Homogenous process ($\text{Fe}^{2+}/\text{H}_2\text{O}_2$). In order to compare the effects of the four parameters considered in the optimization of the oxidative process, a two level Full factorial experimental design (2^4) was utilized using JMP® software. These parameters were concentration of CIP (X_1), concentration of Fe^{2+} (X_2), concentration of H_2O_2 (X_3) and time (X_4) at ambient temperature and an acidic pH. In the optimal conditions of the initial concentration of CIP 10 mg/l, Fe^{2+} concentration of 5 mM, and H_2O_2 concentration of 25.6 mM degradation efficiency of CIP was 76% within 45 min. Under these conditions, the highest correlation coefficient proved between observed and predicted degradation efficiencies with $R^2= 0.996$ and $\text{Adj-}R^2=0.968$. The reaction intermediates have been identified by LC-MS and BOD_5/COD ratio for study biodegradability enhanced from zero to 0.32, showed that the Fenton Homogenous process was agreeable to biological treatment. Based on the results, this may be concluded that Fenton Homogenous process by Full factorial experimental design could be used to degrade CIP from aqueous solutions efficiently.

Keywords: Full factorial design, Degradation efficiency, Fenton Homogenous process, Ciprofloxacin antibiotic, Optimization

1. Introduction

Pharmaceutical residues are important issues to the environment, especially water resources, because they are stable and do not degrade in the environment, even in small concentrations or with low residual activities (Gagnon *et al.*, 2008; Dirany *et al.*, 2010). More specifically, antibiotics are important pharmaceutical pollutants which

may enter water resources through pharmaceutical wastewater, hospital and veterinary clinics sewage, combined with domestic sewage, and effluents of agricultural product plants and fish ponds (Wynnae, 2003).

A big family of antibiotics widely used in disease treatments is Fluoroquinolones, which include Ciprofloxacin (CIP), Ofloxacin and Norfloxacin. The presence of fluorine atoms in the composition of these antibiotics has granted them stability, and therefore they have been considered as a serious contaminant into environment (Capriotti *et al.*, 2012). In particular, CIP is a pharmaceutical antibacterial drug used worldwide in both human and animal medicine for bacterial infections (Zhang *et al.*, 2015; Salari *et al.*, 2018). Ineffective removal of CIP by conventional water treatment technologies and its subsequent discharge into the environment has granted its presence in surface water, groundwater, wastewater, and even plants (Han *et al.*, 2015). Recent studies have shown that advanced of each new pharmaceutical drug mainly antibiotics imposes a potential danger for both human health and environment particularly, hydrology resources (Guo *et al.*, 2013).

Due to poor biodegradability of CIP with biological methods, it looks important to utilize a treatment process that is capable of destroying residual CIP. It is essential to develop modern fast and cost-effective methods to treat pharmaceutical wastewaters (Salari *et al.*, 2018). In fact, removal of this pollutant has been sought by many researchers utilizing many advanced oxidation processes (AOPs). AOPs are effective processes, based on formation of hydroxyl radical, that totally decompose organic and refractory compounds such as CIP to low molecular weight compounds (Pera-Titus *et al.*, 2004). Lately, AOPs have been accepted as efficient methods used for degradation of toxic and environmentally-resisting organics compounds (Giri and Golder 2014; Bouasla *et al.*, 2010). A literature survey shows that degradation efficiency of CIP has been investigated via HPLC¹ and TLC (Krzek *et al.*, 2005). UV and UV/ H_2O_2 by multiple-wavelength ultraviolet light-emitting diodes (Ou *et al.*, 2016), Photo catalytic synthesized with

¹High Performance Liquid Chromatography

TiO₂ nanoparticles on montmorillonite (Hassani *et al.*, 2015), UV/H₂O₂ (Baissa, 2016), photo-Fenton Homogenous (Bobu *et al.*, 2015), Sonolysis (De Bel *et al.*, 2009), and adsorption processes (Jiang *et al.*, 2009). Particularly, Fenton Homogenous processes have been used as one of the best methods to control and reduce organic pollutions, whereby inexpensive and environmentally friendly reagents are employed (Biglarijoo *et al.*, 2016).

While degrading organic compounds, many different variables affect a Fenton Homogenous process such as speed of shaking, pH of the solution, concentration of hydrogen peroxide, volume of the solution, concentration of ferrous ions, contact time, and temperature (Elhalil *et al.*, 2016). Studying effect of each factor separately and interaction of parameters would be quite very tedious and time consuming. Factorial experimental design has been utilized to minimize the above problems with optimizing all affecting parameters collectively at one time (Wang *et al.*, 2010). The design determines the effect of each factor, and interacting effects of the parameters on the response, as well as how the effect of each factor varies with a change in the level of other factors (Arenas *et al.*, 2006). It is known that interaction effects of different factors may be attained only by design of experiments, and factorial method may be applied to reduce the number of experiments, time of experiments, overall process cost, and to achieve a better response (Barka *et al.*, 2014).

In previous studies, most researchers concentrated on evaluating AOPs for degradation of antibiotics, but experimental optimization using Full factorial method and Fenton Homogenous process particularly For CIP antibiotic has been never reported. In this work, an optimization has been done using a 2⁴ factorial experimental design. The full factorial was designed with four factors of two levels. The effects of each factor and their interaction are studied. The main purpose Fenton reaction as a pretreatment method is to improve the BOD₅/COD ratio; thus, the ratio was measured after degradation in optimal condition to estimate the biodegradability rise and intermediates (by-products) were identified by HPLC coupled with a Mass Spectrometer analyses (LC-MS).

2. Materials and methods

2.1. Chemicals and reagents

Ciprofloxacin is an antibiotic compound belonging to a group of drugs called Fluoroquinolones, whose structural formula is presented on Fig. 1 (Kassab *et al.*, 2005; Xiong *et al.*, 2017).

All reagents used in all experiments had analytical grades. CIP was purchased from a local supplier called Shiraz Serum pharmaceutical company. Its Physico-chemical properties are listed in Table 1.

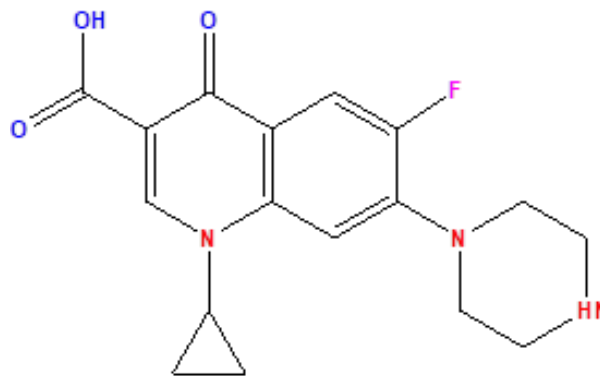


Figure 1. Structural formula of Ciprofloxacin (IUPAC name: 1-cyclopropyl-6-fluoro-4-oxo-7-(piperazin-1-yl)-quinoline-3-carboxylic acid) (Kassab *et al.*, 2005; Xiong *et al.*, 2017)

Distilled water utilized as the solvent to prepare all solutions. A stock standard solution of Ciprofloxacin (500 mg/l) was prepared by suitable dilution of 2ml HCl. Ferrous sulfate (FeSO₄·7H₂O), sulfuric acid (H₂SO₄ (95–7%)), Sodium hydroxide (NaOH) and Hydrogen Peroxide H₂O₂ (30%) were all purchased from Merck Company.

Table 1. Physical-chemical properties of Ciprofloxacin (Xiong *et al.*, 2017)

Properties	Ciprofloxacin
Molecular structure	C ₁₇ H ₁₈ FN ₃ O ₃
CAS Reg. No.*	85721-33-1
Molecular mass (g.mol ⁻¹)	332
Water solubility	30 mgmL ⁻¹ at 20 °C
log Kow**	0.28
λ _{max}	275
pKa	5.90: 8.89
Therapeutic group	Antibiotic
Therapeutic class	Fluoroquinolones

*CAS Registry Number, **Octanol-water partition coefficients (KOW)

2.2. Utilized devices

Most analytical methods and researches use HPLC for determination of CIP concentration in solutions. Also, some researchers have reported use of UV or fluorescence for determination of CIP concentrations (Carlucci, 1998; Wright *et al.*, 2000; Yorke and Froc, 2000). Recently, some studies have reported employing UV-Visible detection for various contaminants (Wright *et al.*, 2000; Kamberi *et al.*, 1998; Maya *et al.*, 2001; Abdennouri *et al.*, 2010). Use of UV-Visible has several advantages, compared to HPLC, such as simplicity, quickness and surely cheaper instrumentation. In this work, all absorbance and concentration measurements were made by a Hach UV-Visible spectrophotometer model no. DR-5000 with 4 ml matched quartz cells.

2.2.1. HPLC/MS

Identification of primary intermediates were recognized by a system of liquid chromatography coupled with a mass spectrometer (LC-MS) (Waters Alliance 2695 HPLC-Micromass Quattro micro API Mass Spectrometer equipped with a Eclipse XDB-C18 5μ, 4.6×150 mm).

The mobile phase was composed of water containing 0.1% formic acid (v/v) and acetonitrile containing 0.1% formic acid (v/v) and the flow rate was 0.5 mL/min. The injection volume was 20 μ L and the column temperature was 30 °C. For MS analysis, ionization was conducted through positive-mode electrospray ionization (ESI+) with a full scan from 50 m/z to 1000 m/z under the following conditions: capillary potential 4 kV, cone voltage 35 V, source temperature 110 °C, desolvation temperature, 300 °C.

2.3. Fenton Homogenous reaction

In recent years, advanced oxidation processes have been used to reduce pollutions caused by the presence of pharmaceutical compound residues in water without producing any secondary toxic contaminants in the environment (Garoma *et al.*, 2010). Fenton Homogenous, firstly discovered in the 1890s. Fenton Homogenous reaction initiates with addition of both iron and hydrogen peroxide to remove various contaminants (Wang *et al.*, 2010). Significant advantages of Fenton Homogenous method include high efficiency, biodegradability enhancement, simplicity in operation and flexibility (Biglarijoo *et al.*, 2016). Conventional Fenton Homogenous process takes benefit of reagents (H_2O_2 as oxidant and $FeSO_4 \cdot 7H_2O$ as catalyst) and utilized to treat refractory wastewaters (Alver *et al.*, 2015). Fenton Homogenous reaction steps are shown in Eqs. (1-5):



Table 2. Calibration data with nine concentrations and their corresponding absorbance values

Concentration (mg/l)	Absorbance (Au)
1	0.10
2	0.20
3	0.33
4	0.40
5	0.50
6	0.59
7	0.65
8	0.72
9	0.82

The obtained linear calibration curve, with a high correlation coefficient of $R^2 = 0.9932$. The equation for the curve is $Y = 0.0882X + 0.0376$ where Y is the absorbance (Au) and X is the concentration in mg/l.

2.7. Design of experimental (DOE) and statistical analyses

A statistical methodology was determined for optimize the Fenton Homogenous process. In a 2^f factorial experimental

2.4. Experimental procedures

A stock standard solution of CIP (500 mg/l) was prepared with dissolving 0.5 g of CIP in 1000 mL of distilled water. Other concentrations were prepared by appropriate dilution of the stock solution with distilled water. The degradation tests were performed in a beaker containing 100 mL of CIP solution at the designed concentration. Then, the required mass of ferrous sulfate was added. The Fenton Homogenous reaction was initiated by adding the required volume of hydrogen peroxide (H_2O_2). The mixture was retained at a constant stirring of 120 rpm at room temperature. The pH of the solution was adjusted to 3 by addition of H_2SO_4 (1 M) or NaOH (1M).

2.5. Process analysis

Solution of CIP showed the maximum absorption peak at 275 nm when scanning the wave length range of 190–400 nm using distilled water and Super acid (Fe^{2+} , H_2O_2) as blank. Then, concentrations of CIP were determined using a spectrophotometer at an absorbance of 275 nm. Prior to the measurements, a calibration curve was achieved using standard CIP solution with known concentrations. pH measurements of solutions was done using a WTW (340i; WTW, Germany) pH meter. Efficiency percentage (De%) was determined using:

$$De(\%) = \frac{C_i - C_f}{C_i} \times 100 \quad (6)$$

Where De is the degradation efficiency (%), C_f is the final CIP concentration, and C_i is its initial concentration in the solution.

2.6. Linearity

For determine the calibration curve, samples were prepared with different CIP concentrations and their absorptions were measured (Table 2).

design, f factors are each varied at two levels. For a given combination of the f factors, more than one test may be performed. Therefore, the total number of tests is given as: $N = 2^f + C$, where C represents the number of center-point measurements used to test the low-to-high range. Center points are simply experimental runs where X 's are set halfway in between (i.e., in the center of) the low and high settings (Elhalil *et al.*, 2016). In the present work

$N = 17, (f = 4, C = 1)$. The polynomial equation based on the first-order model with four parameters (X_1, X_2, X_3 and X_4) and their interaction terms may be given as:

$$De = b_0 + b_1X_1 + b_2X_2 + b_3X_3 + b_4X_4 + b_{12}X_1X_2 + b_{13}X_1X_3 + b_{14}X_1X_4 + b_{23}X_2X_3 + b_{24}X_2X_4 + b_{34}X_3X_4 + b_{123}X_1X_2X_3 + b_{134}X_1X_3X_4 + b_{234}X_2X_3X_4 \quad (7)$$

As mentioned, the influence of four main parameters at a PH of ~ 3 was studied in the present research; concentration of CIP (X_1), ferrous ions (X_2), hydrogen peroxide (X_3), and time (X_4). Suitable experimental values measured during pre-tests in a Fenton Homogenous process (Fe^{2+}/H_2O_2) for degradation of Ciprofloxacin in aqueous solution are shown in Table 3. The range of these

Table 3. Suitable experimental values for the independent variables

Coded symbol	Experimental variable (unit)	Coded values		
		Min value (-1)	Central point (0)	Max value (+1)
X_1	Concentration of Ciprofloxacin (mg/l)	10	45	80
X_2	Concentration of ferrous ions (mM [*])	5	7.5	10
X_3	Concentration of hydrogen peroxide (mM [*])	25.6	38.4	51.2
X_4	Time (min)	15	30	45

*mM=miliMolar

3. Results and discussion

3.1. Degradation efficiencies

The experimental matrix designed by Full factorial method, coded and real variable, and degradation efficiencies are all

parameters was selected according to literature and preliminary experiments (Elhalil *et al.*, 2016).

Results were analyzed with 95% confidence intervals using JMP[®] 11.0.1 statistical discovery software from Statistical Analysis Systems (SAS).

shown in Table 4. Two replications were used for each sample and their mean are presented in this table. As shown, the highest and lowest efficiency was observed at experimental no. 13 and no. 5 respectively. Apparently, CIP concentration and H_2O_2 concentration as a strong oxidizer had the highest influence on CIP degradation.

Table 4. The experimental matrix designed by Full factorial method, variables, and efficiencies

Experiment	Coded variable				Actual variable				First run	Second run	De* (%) (Average of two runs)	Predicted De (%)
	X_1	X_2	X_3	X_4	[CIP]	[Fe ²⁺]	[H ₂ O ₂]	[Time]				
1	-1	1	1	-1	10	10	51.2	15	65.8	68.2	67.1	54.0
2	1	1	1	1	80	10	51.2	45	50.8	60.6	55.7	58.0
3	-1	1	1	1	10	10	51.2	45	60	76	68	64.0
4	0	0	0	0	45	7.5	38.4	30	52.1	56.1	54.1	55.4
5	1	-1	-1	-1	80	5	25.6	15	25.1	33.1	29.1	35.2
6	-1	1	-1	-1	10	10	25.6	15	48.3	52.3	50.3	51.0
7	-1	-1	-1	-1	10	5	25.6	15	65	67	66.0	67.0
8	1	-1	1	-1	80	5	51.2	15	55.2	59.2	57.2	56.6
9	-1	-1	1	1	10	5	51.2	45	69	76	72.5	71.8
10	1	1	-1	-1	80	10	25.6	15	55.4	57.4	56.4	51.0
11	-1	-1	1	-1	10	5	51.2	15	53	55	54.0	50.5
12	1	1	-1	1	80	10	25.6	45	57.1	67.1	62.12	61.0
13	-1	-1	-1	1	10	5	25.6	45	76	80	76	68.0
14	1	-1	1	1	80	5	51.2	45	55.1	61.1	58.1	55.0
15	1	-1	-1	1	80	5	25.6	45	33.8	35.8	34.8	34.0
16	-1	1	-1	1	10	10	25.6	45	43	55	49.0	52.0
17	1	1	1	-1	80	10	51.2	15	57.4	47	52.2	48.0

*De: Degradation efficiency (%)

By substituting the coefficients b_i in Eq. (8), De model can be expressed as:

$$De = 56.62 - 6.07X_1 + 0.18X_2 + 3.81X_3 + 2.74X_4 - 5.08X_1X_2 + 1.28X_1X_3 - 0.76X_1X_4 - 0.67X_2X_3 - 1.64X_2X_4 + 0.23X_3X_4 - 7.08X_1X_2X_3 - 1.98X_1X_3X_4 - 0.23X_2X_3X_4 \quad (8)$$

3.2. Main effects

Based on Equation (8), it was noted that a parameter concentration of CIP is negative; means that negative effects on the response. Other factors, concentrations of CIP, ferrous ion, hydrogen peroxide and the time having positive effects means that high-level parameters are more important in the contaminants removal. It is known that reduction of the contaminant is basically proportional to H_2O_2 and its breakdown to OH^\bullet . Any extra Fe ion would react with the hydroxyl radical and reduce efficiency of the procedure in Equation (9) (Oliveira *et al.*, 2006; Joseph *et al.*, 2000).



In concentrations greater than the optimal amount occurred decomposition of hydrogen peroxide into oxygen and water. Therefore, it may be concluded that too high a concentration of H_2O_2 acts as an inhibitor for the formation of OH^\bullet , and consequently, reduce efficiency of the process; a phenomenon reported in the literature as well (Fu *et al.*, 2007).

3.3. Interactions among factors

Interactions among parameters are shown at low and high levels of all parameters on Fig. 2. The figure indicates that most important interactions exist among (X_1 and X_2), (X_2 and X_1, X_3) and (X_4 and X_1, X_3). For example, the box associated with Fe^{2+} and H_2O_2 considers the interaction of low and high levels of the rate variable (Fe^{2+}) for both levels of H_2O_2 (-1 and 1). The pink line represents the low and the blue line the high level of H_2O_2 . The two lines cross, indicating that there is an interaction among Fe^{2+} and H_2O_2 . Parallel and non-crossing lines indicate that there is no interaction among considered parameters.

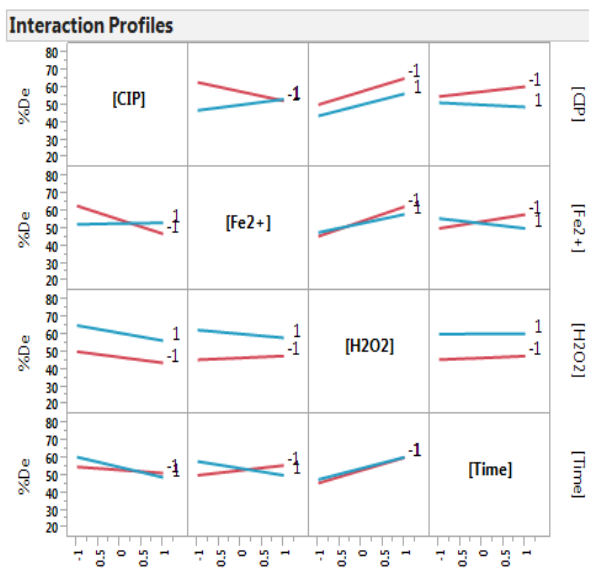


Figure 2. Plots for interactions among parameters affecting CIP degradation efficiency (De)

A 3D plot of the response surface (degradation efficiency) for every two interacting parameters may be drawn at the

optimal condition. Such surfaces for CIP- Fe^{2+} , CIP- H_2O_2 and Fe^{2+} - H_2O_2 are shown on Figs. 3, 4, and 5 respectively. As shown on Fig. 3, degradation efficiency increases with decreasing CIP and/or decreasing Fe^{2+} concentrations. However, as shown on Fig. 4, degradation efficiency increases with decreasing CIP but with increasing H_2O_2 concentrations. Fig. 5, reflects a somewhat similar conclusion where response surface increases with decreasing Fe^{2+} and/or increasing H_2O_2 .

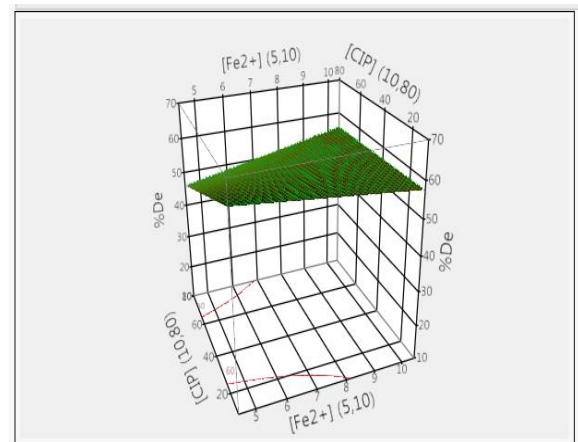


Figure 3. 3D plot of the response surface as a function of [CIP] and $[Fe^{2+}]$ ($[H_2O_2] = 26.5$ mM; Time = 45 min)

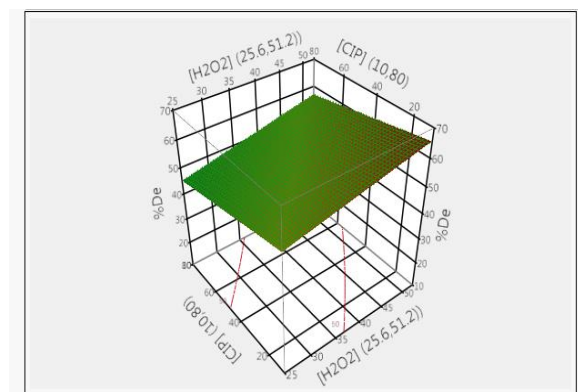


Figure 4. 3D plot of the response surface as a function of [CIP] and $[H_2O_2]$ ($[Fe^{2+}] = 5$ mg/l; Time = 45 min)

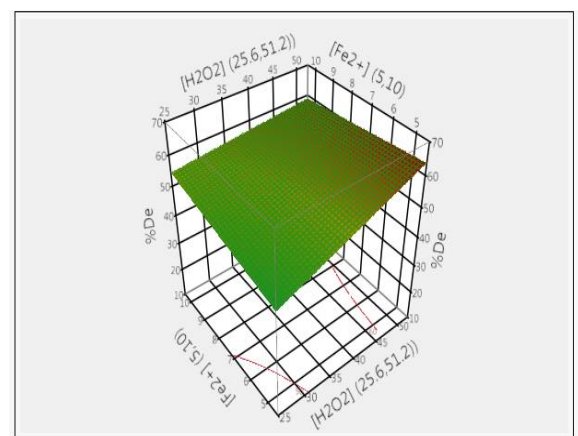


Figure 5. 3D plot of the response surface as a function of $[H_2O_2]$ and $[Fe^{2+}]$ ($[CIP] = 10$ mg/l; Time = 45 min)

3.4. Analysis of variance (ANOVA)

Assess the accuracy of the model is investigated with the analysis of variance (ANOVA) based on a Full factorial design, and the results are presented in Table 5. The main and interacting effects of each factor having P-values less than 0.05 are considered as potentially notable. In other

words, the low P-value indices (shown in red) correspond to significant factors such as [CIP], interactions of $[\text{Fe}^{2+}]$, $[\text{H}_2\text{O}_2]$ and [time]. Such factors also have high t-ratios which exceed the blue line threshold on the Table. Considering only the main factors, it may be concluded concentration of CIP, H_2O_2 , interactions of Fe^{2+} and time are important, respectively.

Table 5. ANOVA test results for important factors affecting degradation percentage based on a Full factorial design

Sorted Parameter Estimates				
Term	Estimate	Std Error	t Ratio	Prob> t
[CIP] (10,80)	-6.07875	0.603957	-10.06	0.0097*
[Fe2+] (5,10)	0.81875	0.603957	1.36	0.3080
[H2O2] (25.6,51.2))	3.81625	0.603957	6.32	0.0241*
[Time] (15,45)	2.74625	0.603957	4.55	0.0451*
[CIP] (10,80)*[Fe2+] (5,10)	5.08375	0.603957	8.42	0.0138*
[CIP] (10,80)*[H2O2] (25.6,51.2))	1.28125	0.603957	2.12	0.1679
[CIP] (10,80)*[Time] (15,45)	-0.76875	0.603957	-1.27	0.3310
[Fe2+] (5,10)*[H2O2] (25.6,51.2))	-0.67125	0.603957	-1.11	0.3821
[Fe2+] (5,10)*[Time] (15,45)	-1.64125	0.603957	-2.72	0.1129
[H2O2] (25.6,51.2))*[Time] (15,45)	0.23125	0.603957	0.38	0.7387
[CIP] (10,80)*[Fe2+] (5,10)*[H2O2] (25.6,51.2))	-7.08125	0.603957	-11.72	0.0072*
[CIP] (10,80)*[Fe2+] (5,10)*[Time] (15,45)	1.96875	0.603957	3.26	0.0826
[CIP] (10,80)*[H2O2] (25.6,51.2))*[Time] (15,45)	-1.10875	0.603957	-1.84	0.2078
[Fe2+] (5,10)*[H2O2] (25.6,51.2))*[Time] (15,45)	-0.23125	0.603957	-0.38	0.7387

3.5. Validity of the model

Observed efficiencies (D_e) for degradation of CIP were plotted against predicted ones (Fig. 6.), reflecting an excellent match. Analysis of variance (ANOVA) based on Full factorial design is also shown on Table 6. As shown, predicted values match the experimental ones well with an $R^2=0.996$, indicating that 99.6% of the variations for D_e (%) are explained by the independent variables. Adjusted R^2 ($\text{Adj-}R^2$), a modified version of R-squared adjusted for the number of predictors in the model, may be more suitable for comparing models with different numbers of independent variables (Guoqiang *et al.*, 2017). Also, F-ratio is notable in Table 6, indicating that the model adopted in this study (full factorial design) is acceptable and validated.

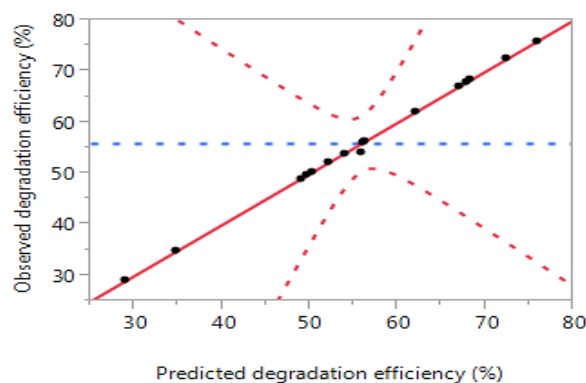


Figure 6. Predicted vs. observed efficiencies for degradation of Ciprofloxacin

Table 6. Analysis of variance (ANOVA) based on Full factorial design results

Source	Degree of freedom	Sum of squares	Mean squares	F- Ratio
Model	14	2342.1	167.2	36.22
Pure Error	2	9.23	1.653	-
C. Total	16	2351.3	-	-
$R^2=0.996$	$R^2_{\text{adj}}=0.968$	-	-	-

3.6. Identification of primary intermediates

To illuminate the degradation mechanism of CIP in the Homogeneous Fenton process system and thus to show a possible reaction pathway, a mass spectroscopy study was carried out to determine the intermediates in aqueous solution. The intermediates during CIP degradation detected by the peaks formed using HPLC-MS. Table 7 summarizes molecular structure and m/z values of four

primary intermediates compound identified by this technique.

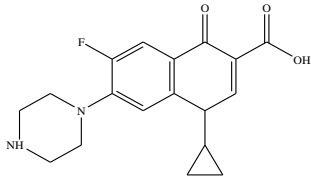
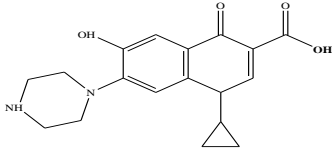
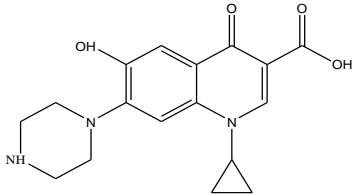
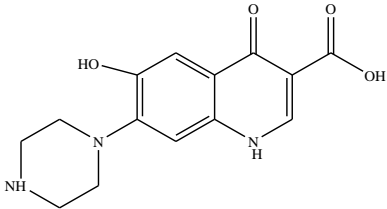
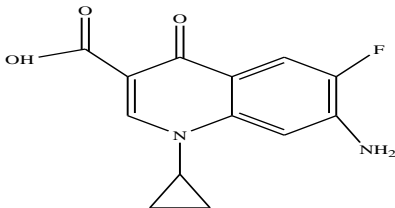
A noteworthy alternative to completing oxidation through chemical methods is the utilize of a chemical pre-treatment process for the conversion of biodegradable acids initially through biodegradation reactions, also to broken into biodegradable intermediates, and then the biological

oxidation of these intermediates to simpler compounds such as biomass and water.

For example, organic macromolecules, such as resistant organic compounds of soluble in water, by chemical oxidation might break into smaller intermediate compounds (such as short-chain organic acids) that are easily degraded from the original molecules, so the biological oxidation rate increases with decreasing molecular size (Abbasi, 2009).

It should be noted that, complete degradation of these intermediates to water and CO₂ (carbon dioxide) is difficult because of decreasing division rate of C-C bond by decreasing molecular size of them. So, chemical oxidation and biological treatment as pre-treatment and post-treatment, respectively for resistant organic compounds are practically useful (Mantzavinos and Psillakis, 2004). Results of biodegradable intermediates assessed based on BOD₅/COD ratio shows that Fenton Homogenous method can be utilized for greater improvements of biodegradability which enhanced from zero to 0.32.

Table 7. Identification of the CIP degradation intermediates by HPLC–MS

Compound	Retention time (min)	m/z	Proposed structure
CIP	2.56	332	
1	2.83	330	
2	3.12	334	
3	3.15	287	
4	3.21	263	

We should also note that there may be other intermediate products as well. Due to well-known intermediate products, we concluded that the proposed method can be accepted for complex compound organic compounds as a pre-treatment method.

4. Conclusions

Full factorial method, the only means to completely and systematically study interactions between factors in addition to identifying significant ones, utilized to design a

test and determine optimum conditions for CIP degradation by Fenton Homogenous method. It is known that one-factor-at-a-time experiments (where each factor is investigated separately by keeping all the remaining factors constant) do not reveal the interaction effects between the factors. Full factorial design focused on relationships among process variables to maximize the impact and determine the optimal conditions for better degradation of CIP. The experimental system used in present study was discontinuous, and concentration of the

antibiotic was detected using UV-visible spectrophotometric as opposed to other devices that had been used in previous studies. The use of this device has important advantages such as simplicity, speed, high sensitivity, and low cost per analysis.

Based on the results, CIP degradation indeed occurred with Fenton Homogenous process, and hence, it may be utilized as a pretreatment process for antibiotics in aqueous solution. Statistical analysis results show that optimal conditions for the highest CIP degradation in polluted water are pH= 3; [CIP]= 10 mg/l; [Fe²⁺]= 5mM; [H₂O₂]= 25.6 mM, where a maximum degradation efficiency of 76% occurred in 45 min. An excellent correlation between predicted and observed degradation efficiencies was obtained, confirming validity and practicability of the adopted model with R²=0.996 and Adj-R²=0.968. In addition, results show that all parameters were important in the analysis and degradation of the antibiotic, however with different levels of importance, ranking from the highest (initial concentration of CIP and concentration of H₂O₂) to the lowest important ones (concentration of Fe²⁺ and time). The result of BOD₅/COD ratio shown that biodegradability enhanced from zero to 0.32, demonstrating the effluent Fenton Homogenous process can be applied to biological treatment.

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